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Use of Multiple Linear Regression Technology in Controlling the Technical Specifications of Industrial Products: Predicting the Mechanical Specifications of the Products of the Longitudinal Rolling Factory of the LISCo

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ABSTRACT

The main objective of this study is to arrive at the formulation of a model through which to predict the mechanical specifications of the products of the longitudinal rolling mill of the Libyan Iron and Steel Company (LISCo), using the multiple linear regression method, and in a simple, accurate manner through which the quality of the products can be controlled within the specifications approved by the LISCo Given the proportions of the added chemicals As a conclusion, the mechanical specifications of the products were predicted from yield stress, tensile strength and elongation ratio, and the error rate in predicting these mechanical specifications was very close to zero. This research also contributes to introducing the LISCo to the importance of prediction models for mechanical properties, which work to reduce the rate of uncertainty, especially with the development of forecasting methods that allow improving the degree of accuracy and help in making sound decisions.

إستخدام تقنية الانحدار الخطي المتعدد في التحكم في المواصفات الفنية للمنتجات الصناعية (التنبؤ بالمواصفات الميكانيكية لمنتجات مصنع الدرفلة الطولية بالشركة الليبية للحديد والصلب)

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الملخص

الكلمات المفتاحية: الانحدارالخطي الشركة الليبية للحديد والصلب منتجات صناعية توقعات

سعينا من خلال هذه الدراسة للوصول إلى صياغة نموذج يمكن من خلاله التنبؤ بالمواصفات الميكانيكية، لمنتجات مصنع الدرفلة الطولية بالشركة الليبية للحديد والصلب، باستخدام طريقة الانحدار الخطي المتعدد، وبأسلوب بسيط، ودقيق يمكن من خلاله ضبط جودة المنتجات في حدود المواصفات المعتمدة لدى الشركة الليبية للحديد والصلب، بمعلومية نسب المواد الكيميائية المضافة حيت تم التنبؤ بالمواصفات الميكانيكية للمنتجات من اجهاد خضوع وقوة شد ونسبة الاستطالة وكانت نسبة الخطأ في التنبؤ بهذه المواصفات الميكانيكية قريبة جداً لصفر. كما يسهم هذا البحث في تعريف الشركة الليبية للحديد والصلب بأهمية نماذج التنبؤ التي بالخواص الميكانيكية، التي تعمل على التخفيض من نسبة عدم التأكد، خاصة مع تطور أساليب التنبؤ التي تسمح بتحسين درجة الدقة، وتساعد في اتخاذ القرارات السليمة.

1. Introduction:

The industrial and technological development depends largely on the progress in the field of products and their quality, and as a result of

this great industrial development that the world witnessed in all fields, the need arose to know the mechanical properties of materials

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E-mail addresses: o.azuza@eng.misuratau.edu.ly, (Madi Naser) m.naser@eng.misuratau.edu.ly Article History : Received 26 May 2021 - Received in revised form 21 October 2021 - Accepted 08 November 2021 with multiple industrial uses so that these characteristics have high quality specifications in terms of resistance to pressure, durability, and submission Tensile, resistance, and mechanical properties in general, in order to predict them, and for their adoption in various industrial applications. The mechanical properties can be divided into the following ^[3]:

Yield Stress: Yield stress is known as the yield point, a point on the stress-strain curve] ^{3]}. Yield strength is a property related to critical materials, which is exploited by many basic techniques of working materials to reshape materials by pressure (such as: forming, rolling, pressing, bending, and hydraulic shaping) to separate materials by cutting (such as using a machine) or shearing, and to connect elements rigidly to fasteners, the yield load is taken It is the load applied to the center of a spring loaded to straighten its plates ^[2].

Tensile Strength: It is a measure of how much stress you dance, dances the right way, which then crashes or loses, crashes or outruns, without crashing and can be calculated by the following equation:

$$\sigma = \frac{r}{A}$$

Where:

- $\sigma:$ tensile strength, unit of measurement (newtons/square meter) (N/m²).
- F: the amount of force, the force that pulls the ends of the metal together, the unit of measure (newtons) (N).
- A: The cross-sectional area of the metal, unit of measure (square meters) (m^2) .

Elongation Ratio: It is a measure of the ductility of a material and is defined from the following equation ^[3]:

$$\varepsilon = \frac{\Delta L}{Lo} = \frac{L - Lo}{Lo}$$

Where:

ε: elongation ratio.

 ΔL : the increase in length.

Lo: is the original length.

L: is the final length.

Prediction/ Forecasting:

Forecasting is the mainstay for the internal planning of the company's policy decisions, as most of the administrative decisions in the facility depend on forecasting directly or indirectly.^[4].

Reasons for the rapid spread of the use of forecasting:

Forecasting is based on a number of factors, the most important of which are [4]:

- Continuous progress in models and methods of forecasting.
- Increasing the volume and complexity of the administration's work, which made it more difficult to deal efficiently with decision-making without relying on models that facilitated unraveling the ambiguities of the future.
- The administration has become completely convinced at the present time of the advantages resulting from the use of forecasting, and its feasibility in completing planning processes.
 Forecasting Requirements:

Forecasting depends on a set of requirements, the most important of which are ^[5]:

- Interest in and familiarity with various past historical records related to the demand forecasting process.
- List the factors that affect the sales volume in the past, such as income, advertising, commodity quality and price.
- Develop a visualization of the future activity of sales.
- Review and correct predictions and evaluation for future feedback.
- Determining the dependent demand and the independent demand.
- Attention and full knowledge of competing and alternative goods and their development.
- Taking into account the life cycle of the commodity, while forecasting sales, and at what stage of the cycle the commodity will be, where sales are at their peak in a phase of saturation and this phase is characterized by a degree of relative stability in sales, and in this phase it is necessary to seek the assistance of

experts to create new benefits for the commodity, to increase the demand for it, otherwise the commodity will go into decline.

Steps To Prepare The Forecast:

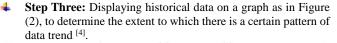
Preparing the forecast is by following these steps ^[5]:

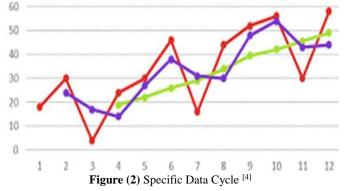
First Step: Determining the purpose of the forecasting process, [5].

Step Two: Collecting historical data, whether on economic trends from government documents, and Figure (1) illustrates how to collect data ^[5].

Φ	Weight				Area of	Crose -	Section	in Cm ₂			
nm	kg/m	1	2	3	4	5	6	7	8	9	T
5	0.154	0.196	0.393	0.589	0.785	0.982	1.18	1.37	1.57	1.77	1 1
6	0.222	0.283	0.566	0.848	1.13	1.41	1.70	1.98	2.26	2.54	2
7	0.302	0.385	0.770	1.15	1.54	1.93	2.31	2.69	3.08	3.46	3
8	0.395	0.503	1.01	0.51	2.01	2.51	3.02	3.52	4.02	4.52	5
10	0.617	0.785	1.57	2.36	3.14	3.93	4.71	5.50	6.28	7.07	7
12	0.888	1.13	2.26	3.39	4.52	5.65	6.79	7.92	9.05	1.02	11
13	1.04	1.33	2.66	3.98	5.31	6.64	7.96	9.29	10.6	11.9	1:
14	1.21	1.54	3.08	4.62	6.16	7.70	4.24	10.8	12.3	13.9	1
16	1.58	2.01	4.02	6.03	8.04	10.1	12.1	14.1	16.1	18.1	2
18	2.00	2.54	5.09	7.63	10.2	12.7	15.3	17.8	20.4	22.9	2
19	2.23	2.835	5.67	8.50	11.30	14.2	17.0	19.9	22.7	25.5	2
20	2.47	3.14	6.28	9.42	12.6	15.7	18.8	22.0	25.1	28.3	3
22	2.98	3.80	7.60	11.4	15.2	19.0	22.8	26.6	30.4	34.2	3
24	3.55	4.52	9.04	13.6	18.1	22.6	27.0	31.7	36.2	40.7	4
25	3.85	4.91	9.82	14.7	19.6	24.5	29.5	34.4	39.3	44.2	4
26	4.17	5.31	10.6	13.9	21.2	26.5	31.9	37.2	42.5	47.0	5
28	3.83	6.16	12.3	18.5	24.6	30.8	37.0	43.1	49.3	55.4	6
30	5.55	7.07	14.1	21.2	28.3	35.3	42.4	49.5	56.6	63.6	7
32	6.31	8.04	16.1	24.1	32.2	40.2	48.3	56.3	64.3	72.4	8
34	7.13	9.08	18.20	27.2	36.3	45.4	54.5	53.6	72.6	81.7	9
36	7.99	10.2	20.4	30.6	40.8	50.7	61.2	71.4	81.6	91.8	1
38	8.9	11.3	22.6	33.9	45.2	56.5	67.8	79.1	90.4	102	1 1

Figure (1) Data Collection Form [5]





- Step Four: Choosing a forecasting model. There are three main methods of forecasting: time-series models, causal models, and qualitative models. In general, we find that time-series models use historical data for the thing to be predicted to predict future demand values. These models depend on the study of the previous behavior of factors over time and we conclude including what will be in the future, and causal models are used for data on independent variables to develop predictions for dependent variables ^[5].
- Step Five: Conducting experiments that show the correctness of the methods that were used to predict the real values that appeared during the past period, and the method that produces the smallest average error is usually used, and you use it to predict the coming period. There are common measures to measure the error shown in Figure 3, which are the bias error and the average Absolute deviation and relative error, and when the number of the sample is 30 or more, we can judge that the distribution of samples is a normal distribution, and the distribution of the estimate of the standard deviation of the community ^[5].

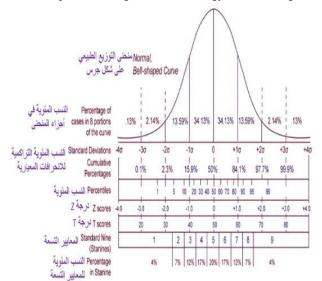


Figure 3 Error Measures ^[5]

- Step Six: The forecast method is used to predict the values of the dependent variables after their occurrence during the forecast period. It is noted here that statistical methods can be applied to create a reliable level of analysis.
- Seventh Step: Incorporating the effect of information on internal and external factors.
- Step Eight: Follow up on the results of applying the forecast method by recording the actual performance and observing the forecast error.

Forecasting Methods and Models:

1. Quantitative Methods:

Quantitative forecasting methods depend on the use of past data to predict the future, and this is consistent with the popular saying, $^{[6]}\!\!\!\!$

A. Time Series Analysis:

The main objective of time series analysis is to identify the changes of the time series and to deconstruct this series in order to make an accurate forecast.

B. Regression and Correlation Analysis Models:

Regression analysis is one of the basic statistical methods in predicting the behavior of economic phenomena in the long run. $^{[6]}\!\!\!\!$

1. Simple Regression Analysis Models:

The relationship between the dependent variable and the independent variable is linear, and the regression Equation is as follows and as shown in the Figure (4).

$$Y=a+bx+\mu$$

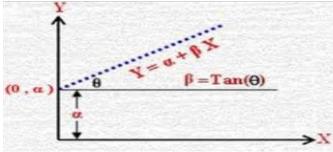
Y: the dependent variable.

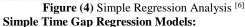
X: the independent variable.

 $\boldsymbol{\mu} {:}$ the amount of error.

a,b: coefficients.

2.





It often occurs in economic life in the time mismatch between cause and effect, such as the slowing down of the effect of new equipment on the quantity of production, and this issue is called the time delay of the effect of one phenomenon on another, and when taking into account the amount of time units of slowdown, the simple regression model with time gap gives In the following form ^[7]:

$$\hat{y}_1 = a + bx_{t-L}$$

Where:

Y: the dependent variable.

X: the independent variable.

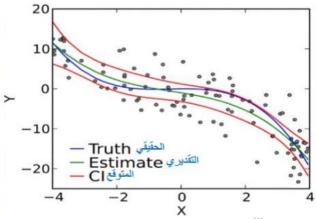
L: the amount of time units of deceleration (the length of the time gap).

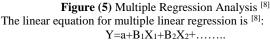
t: time.

a, b: coefficients.

3. Multiple Regression Analysis Models:

Multiple linear regression is one of the advanced statistical methods, which ensures the accuracy of inference in order to improve research results through optimal use of data in finding causal relationships between the phenomena of the research subject, as shown in Figure (5)^[8].





Whereas.

Y: dependent variable

a: constant value

B1: the slope of the y regression on the first independent variable

- B₂: the slope of the y-gradient on the second independent variable
- X₁: the first independent variable
- X₂: The second independent variable

Multiple linear regression can be used if the following conditions are met ${}^{[8]}$:

- The relationship between the independent variables and the dependent variable must be linear.
- The data should be normally distributed for the independent variables and the dependent variable.
- The values of the dependent variable must be of at least ordinal level.

After obtaining the results of the multiple regression equation, we must show whether these coefficients are statistically acceptable. In order to judge the significance of the regression coefficients, we use the test (T) and the level of probability corresponding to it. It is known that the statistical program (SPSS), which is the program of the statistical and social package, and the language (R) which is a software work environment for computer statistics that allows making statistical applications on the one hand and building statistical programs on the other hand. They will automatically extract a T-test and its corresponding probability level. It will also obtain statistics used to know the overall significance of the model and from it (R), (R2). The first (R) is the simple correlation coefficient, which measures the strength of the relationship between two or more variables, while (R2) is called the coefficient of determination, which is used to find out the explanatory power of the estimated model (estimated equation) in the case of simple linear regression (one independent variable with one dependent variable). [7]

2. Qualitative Methods:

It is a set of objective methods that are used to make a forecast of demand when historical data on demand is not available, and which depends on methods that invest the wisdom and experience possessed by management ^[9]

1.2 Problem of Study:

The LISCo is considered one of the largest industrial companies in Libya, and due to its high production costs in order to guarantee the quality of its products, which forced it to conduct many checks and mechanical tests for its products, starting with the casting process in the furnace factories, and ending with testing the mechanical specifications of its final products, and that In order to control the quality of its products according to international standards.

1.3 Research Hypotheses:

- There is no relationship between the independent variables and the dependent variable.
- There is at least one relationship between the independent variables and the dependent variable.

1.4 Importance of the Study:

The importance of forecasting is prominent in the institution, and its importance increases according to the increase in the activity of the institution and the volume of sales and production operations in it, as the forecast situation affects the plan that is developed by the company's management to determine the volume of activity. In order to ensure the quality of product, the company perform mechanical tests which result in consuming time, materials, labour force, which is result in high costs., therefore this study was proposed to examine the possibility of using the prediction method to save the large sums spent on the tests conducted.

1.5 Objective of the Study:

We seek through this study to reach the formulation of a model through which the mechanical specifications of the products of the longitudinal rolling mill of the LISCo can be predicted using the multiple linear regression method, and in a simple and accurate manner through which the quality of the products can be controlled within the specifications approved by the LISCo.

1.6 Study Methodology:

In order to achieve the objective of the study, the process of collecting data and information was relied on the following:

- Collecting data, recording, and observations through field visits.
- Applying demand forecasting using multiple linear regression method.
- Analyze the results that realize the aim of the study and my lead to further studies in the area.

2. The LISCo:

The LISCo in Libya is considered a relatively new industry. It is considered one of the largest industrial companies in Libya. It contains 10 production factories and 5 basic facilities. In addition to workshops, warehouses and laboratories, the company also has a wire drawing plant in Tripoli, where the annual design capacity of the company's factories is estimated at (1.32 million tons) of liquid steel and (1.1 million tons) of sponge iron, which has been increased to 1.7 million tons of liquid steel and (1.75 million tons) of hot-moulded sponge iron, ^[1].

2.1 Production Units:

The company includes the following production units ^[1]:

- Direct reduction factory (3 units).
- Steel factory (2,1).
- Rolling for bars and skewers factory (4 lines).
- Light and medium sectors rolling factory.
- Hot rolling factory.
- Cold rolling factory.
- 4 Galvanizing line.
- Paint line.

2.2 Supporting Units:

The company includes many auxiliary units and facilities, the most important of which are ^[1]:

- Port and storage yard for pellets.
- Electricity and water desalination plant.
- An oxygen and compressed air factory.
- A lime factory.
- Central workshop.
- A training center.
- Quality control laboratories.
- 4 A resort and a sea club.
- In the context of the company's concern and its tireless quest to

respond to the customer's demands, and to impose its position in the international markets among the international iron and steel companies, it has worked to adopt the International Quality Standard (ISO 9001/2000) system and formed a Quality Council for it, to ensure the effectiveness of its application, and to achieve the desired goals, which qualified The LISCo was awarded the 12th European International Quality Award in 1998. It also obtained the Certificate of Implementing the Total Quality System 9001/2000 (ISO) on March 25, 2002.

2.3. Factories:

2.3.1. New Bar Rolling Factory:

The factory includes one new line for the production of bars with a design capacity of (800 thousand tons) of steel reinforcement, sizes (8 mm to 40 mm), where the factory uses bars of size (130 mm-150 mm). It is worth mentioning that those who operated the factory are national cadres within a month June of the year 2017, and Figure (6) shows the Rolling Bars Factory ^[1].



Figure (6) Bar Rolling Production Factory ^[1] **2.3.2. Hot Strip Rolling Factory:**

The annual design capacity of the factory is (580,000 tons) of hot rolled coils, which are shown in Figure (7), and the commercial operation income is on 05/10/1990.



Figure (7) Products of the Hot Strip Rolling Factory ^[1] **2.3.3. Cold Rolling Factory:**

The commercial operation of the factory began on January 20, 1990, with an annual design production capacity of (140,000 tons) of coldrolled coils, as shown in Figure (8).



Figure (8) Products of the Cold Strip Rolling Factory ^[1] **2.3. Mechanical Properties of the Material:** The concept of mechanical properties of a material is how it behaves

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when loaded, where the elasticity factor of a material affects the amount of deflection under load, and the strength of a material determines the stresses it can withstand before it breaks, where the ductility of a material also plays an important role in determining when a material breaks when it is loaded beyond the limits Their flexibility, and because every mechanical system is subjected to loads during operation, it is important to understand how the materials that make up those mechanical systems behave^[2].

3. Study Status:

The importance of forecasting is due to the fact that the company's long-term existence depends on the existence of a continuous demand for its goods or services, and this demand is linked in some way to the general level of economic activity. All management activities must be planned in advance, as well as all management decisions must be anticipated in the light of forecasts future prospects for this activity.And we seek through this study to reach models through which to predict the mechanical specifications of the products of the longitudinal rolling mill of the LISCo, using the multiple regression method, and in a simple and accurate way through which the quality of the products can be adjusted according to the specifications approved by the LISCo, where we took 198 A sample from the LISCo, to prove the accuracy of the prediction results and compare them with the real results of each of the yield stress, tensile strength and elongation ratio. The stratified sample was selected which is groups (DRI reduced iron group, FeMn group, Ferro silicon group FeSi group, Calcium oxide Lime group, Calcium fluoride group DOL, Carbon group C, Silicon group Si, Manganese group Mn), due to the availability of 198 samples. With great accuracy, Figure (9) shows the samples used in preparing and testing the prediction model.

NO	DRI	FeMn	FeSi	Lime	Dol.	С	Si	Mn	Yield Effort s	Tensile El	ongation
1	0.93647	0.00745	0.00287	0.04363	0.00319	34	23	81	448	747	20
2	0.93779	0.00729	0.00281	0.04897	0.00313	31	19	75	429	668	17
3	0.66688	0.00729	0.00281	0.04168	0.00313	30	20	74	431	681	18
4		0.00753	0.0029	0.0484	0.00323	32	21	70	450	673	21
5		0.00729	0.00281	0.0521	0.00313	30	22	72	475	771	15
6	0.9244	0.00886	0.00342		0.0038	30	19	80	384	619	20
7	0.93579		0.0029	0.04302		31	18	77	412	653	19
8		0.04248			0.00020	29	22	76	412	700	16
9	0.84966		0.0037	0.05482	0	32	21	75	382	583	26
10	0.9289	0.00834	0.00322	0.05955		29	23	79	452	732	16
11	0.75023	0.007	0.0027	0.05002	0.003	33	24	70	428	692	17
12	0.8651	0.00631	0.00243	0.03514	0.0027	30	26	74	442	717	20
13	0.94875	0.00722	0.00278	0.04125	0.00309	32	25	76	419	650	19
14	0.94087	0.00693	0.00267	0.04457	0.00297	35	18	74	442	712	22
15	0.69409	0.00715	0.00276	0.0347	0.00306	33	26	70	444	729	17
16	0.9329	0.00787	0.00303	0.0562	0.00337	34	23	72	394	651	20
17	0.890403	0.007695	0.002968		0.003298	34	21	74	370	613	21
18			0.003508			32	19	68	412	622	21
19					0.003126	31	22	71	408	673	25
					l In Pr				sting th		
20	0.94711	0.00745				31	22	72	418	653	18
21	0.93906	0.00715	0.00276	0.01429		32	21	75	437	697	17
22	0.91695	0.00729	0.00281	0.01563		31	21	70	394	639	20
23 24	0.60376	0.01208			0.00518	29 31	21	86	433 374	655 564	26 21
	0.00057	0.00750	0.0000	0.01000	0.00020		20			004	

25	0.98957	0.00753	0.0029	0.03012	0.00323	35	25	75	410	658	20	
26	0.65127	0.01018	0.00275	0.05495	0.00305	34	14	72	387	595	22	
27	0.96618	0.02196	0.01186	0.24155	0.01318	37	18	66	379	593	21	
28	0.9711	0.00819	0.00316	0.0585	0.00351	30	19	69	370	554	26	
29	0.93779	0.00729	0.00281	0.04168	0.00313	35	21	74	388	609	20	
30	0.93594	0.0113	0.00436	0.04841	0.00484	35	25	73	380	626	20	
31	0.98802	0.00865	0.00333	0.0457	0.00371	25	11	66	365	546	24	
32	0.98989	0.00729	0.00281	0.0521	0.00313	32	20	74	403	651	19	
33	0.95683	0.00761	0.00294	0.05437	0.00326	29	18	81	399	597	18	
34	0.98934	0.00769	0.00297	0.05496	0.0033	35	14	75	409	676	16	
35	0.78927	0.01036	0.00266	0.04933	0.00296	34	19	77	376	608	21	
36	0.739211	0.00761	0.003153	0.043483	0.003261	31	15	98	358	559	22	
37	0.989583	0.007292	0.003125	0.041667	0.003125	43	15	73	401	633	21	

Figure (9-b) Samples Used In Preparing and Testing the Prediction

					Mo	del.					
38	0.70409	0.00761	0.00285	0.04757	0.00285	26	23	62	444	627	16
39	0.98612	0.01053	0.00335	0.04787	0.00287	26	18	68	343	537	23
40	0.97166	0.02227	0.00607	0.08097	0.00607	25	18	75	393	573	24
41	0.34568	0.02963	0.00741	0.07407	0.00741	28	17	78	371	556	22
42	0.98644	0.00986	0.0037	0.04932	0.0037	24	12	98	406	660	19
43	0.70323	0.01125	0.00422	0.07032	0.00422	33	18	1,01	407	681	26
44	0.98806	0.00869	0.00326	0.04886	0.00326	35	16	87	400	626	20
45	0.68985	0.01054	0.00259	0.04791	0.00287	38	2	84	426	664	18
46	0.98872	0.00752	0.00376	0.05373	0.00322	31	24	72	350	542	23
47	0.98684	0.00987	0.00329	0.05482	0.00329	36	19	84	326	499	25
48	0.97959	0.01633	0.00408	0.06803	0.00408	33	17	109	366	565	22
49	0.95238	0.03741	0.0102	0.10204	0.0102	33	21	76	364	584	22
50	0.96691	0.00859	0.00301	0.05372	0.00322	24	26	74	348	537	22
51	0.98253	0.01365	0.00382	0.05459	0.00328	37	21	87	385	608	23
52	0.97986	0.01633	0.00381	0.05444	0.00327	33	18	91	397	598	20
53	0.98793	0.00878	0.00329	0.05488	0.00329	29	13	90	411	626	23

Figure (9-c) Samples Used In Preparing and Testing the Prediction

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 | 54 0.984.6 0.0124 0.00311 0.22 78 392 630 20 56 0.986.91 0.0107 0.0032 0.6030 0.0032 40 18 80 384 619 20 57 0.938.62 0.0107 0.0037 0.037 81 78 94 413 679 25 58 0.98542 0.0164 0.0034 0.0337 0.032 23 12 89 355 632 22 60 0.98166 0.0144 0.0031 0.0537 0.0032 31 12 89 355 632 29 19 61 0.98214 0.0136 0.0611 0.0511 0.0036 33 18 91 390 631 29 18 414 637 220 18 931 664 24 65 26 26 26 26 26 26 26 26 26 26 26 27 15 41 429 62 42 65 18 29 41 43
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 59 355 60 22 60 0.8656 0.0146 0.0036 0.0037 3 12 89 355 632 25 61 0.8224 0.0146 0.0036 0.0036 3 18 91 300 631 20 62 0.8763 0.0146 0.0036 0.0036 3 18 81 449 645 24 64 0.9782 0.0036 0.00376 3 18 81 449 645 24 65 0.9782 0.00376 0.0038 21 19 7407 | 54 0.94446 0.01244 0.00311 0.05181 0.00311 32 24 79 0.052 0.0536 0.0124 0.00311 0.0518 0.0032 0.0032 0.0032 0.0032 0.0032 0.0032 0.0032 0.0032 0.0032 0.0032 0.0173 0.0017 0.0171 0.0172 0.0011 0.0171 0.0171 0.0172 0.0011 0.0171 0.0172 0.0011 0.0171 0.0172 0.0171 0.0172 0.0011 0.0171 0.0172 0.0171 0.0172 0.0011 0.0172 0.0171 0.0172 0.0011 0.0172 0.0171 0.0172 0.0011 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.0172 0.
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17 igure (9-f) Samples Used In Preparing and Testing the Prediction
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17 igure (9-f) Samples Used In Preparing and Testing the Prediction
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| 0.98979 0.00737 0.00284 0.04212 0.00138 35 18 76 425 738 0.98468 0.01204 0.00228 0.04376 0.00128 33 20 92 413 657 0.93468 0.0113 0.00277 0.6135 0.00328 33 20 92 413 657 0.93468 0.0113 0.00277 0.6135 0.00328 36 18 78 384 601 0.98640 0.01176 0.00221 0.0521 33 16 53 376 599 0.70855 0.00729 0.00221 0.0520 0.0031 32 23 81 400 702 0.98979 0.00720 0.0221 0.0500 36 22 82 400 602 0.98947 0.01231 0.00301 34 20 77 418 645 0.9867 0.09926 0.00276 0.05249 0.00313 31 22
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 | 91 0.98979 0.00737 0.00224 0.04212 0.00316 36 18 76 425 738 11
92 0.98468 0.01204 0.00328 0.04376 0.00328 33 20 92 413 667 22
93 0.33458 0.0113 0.00277 0.05135 0.00308 36 18 78 3384 601 21
94 0.98648 0.01166 0.00286 0.05298 0.00318 30 25 81 386 586 22
95 0.98501 0.01178 0.00321 0.0535 0.00313 31 15 83 376 569 22
96 0.70855 0.00729 0.00281 0.0521 0.00313 32 19 76 3669 623 22
98 0.9009 0.07207 0.0270 0.22523 0.02703 36 22 82 400 602 11
99 0.98413 0.0127 0.00320 0.05310 0.0031 32 19 76 3569 623 22
98 0.9009 0.07207 0.0270 0.22523 0.02703 36 22 82 400 602 11
99 0.98413 0.0127 0.0038 0.0521 0.00331 31 20 77 418 645 11
101 0.9867 0.00998 0.0033 0.05643 0.00333 31 22 87 431 673 22
103 0.97297 0.01892 0.00210 0.00330 31 22 87 431 673 25
103 0.97297 0.01892 0.00210 0.00278 0.00246 22 17 64 380 542 22
104 0.98463 0.00276 0.00278 0.00278 0.00246 22 17 44 380 542 2
105 0.7085 0.0079 0.00270 0.0027 0.00238 31 20 77 430 678 22
105 0.0799 0.0072 0.00278 0.00238 31 21 77 430 678 22
107 0.94143 0.00685 0.00276 0.00333 33 21 84 391 677 20
108 0.98040 0.00796 0.00278 0.00328 31 21 77 430 678 22
109 0.98443 0.00685 0.00278 0.00310 0.0033 33 21 77 430 678 22
109 0.98448 0.00858 0.00278 0.00328 31 20 77 430 678 22
109 0.98448 0.00858 0.00278 0.00328 31 21 77 430 678 22
109 0.98948 0.00328 0.00310 0.0031 33 21 77 430 678 22
109 0.98948 0.00328 0.00310 0.0031 33 21 77 430 678 22
109 0.98948 0.00328 0.00310 0.0031 33 21 77 441 641 19
Figure (9-f) Samples Used In Preparing and Testing the Prediction
Model.
108 0.9901 0.007 0.0029 0.00281 0.0031 33 21 70 440 688 19
110 0.9573 0.00328 0.00310 0.0031 33 22 17 70 440 688 19
111 0.95842 0.00310 0.0520 0.00313 22 21 70 4410 688 19
112 0.94767 0.00737 0.00284 0.0438 0.00313 36 20 84 386 665 22
112 0.94767 0.00737 0.00284 0.0438 0.00316 39 32 90 401 661 15
113 0.95863 0.00728 0.00281 0.0478 0.00316 39 32 90 401 661 15
113 0.95863 0.00728 0.00281 0.0478 0.00316 39 32 90 401 661 15
114 0.95642 0.01387 0.00284 0.0438 0.00316 39 32 90 401 661 15
115 0.94767 0.0073 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$
 | 91 0.98979 0.00737 0.00284 0.04212 0.00316 35 18 76 425 738 11
92 0.98468 0.01204 0.00328 0.04376 0.00328 33 20 92 413 667 22
93 0.93468 0.0116 0.0028 0.05298 0.00318 30 25 81 386 667 2
94 0.98548 0.0116 0.0028 0.05298 0.00318 30 25 81 386 669 2
95 0.98501 0.01178 0.00321 0.05535 0.00321 33 15 83 376 569 2
96 0.70855 0.00729 0.00281 0.0521 0.00313 32 19 76 369 623 2
98 0.9009 0.07207 0.0270 0.0222 0.5200 0.00313 32 19 76 369 623 2
98 0.9009 0.07207 0.0270 0.22523 0.02703 36 22 82 400 602 11
99 0.98413 0.0127 0.00310 0.0521 0.00333 31 20 87 431 678 22
100 0.98462 0.01331 0.0038 0.05231 0.00308 34 20 77 448 645 11
101 0.9867 0.00998 0.0033 0.05643 0.00333 31 22 87 431 673 2
103 0.97297 0.01892 0.0021 0.00310 34 25 80 372 560 2
103 0.97297 0.01892 0.0042 0.00390 0.00233 31 22 87 431 673 2
104 0.97872 0.01702 0.0042 0.00790 0.0032 9 22 292 419 654 11
106 0.98645 0.00796 0.00276 0.00276 0.00228 31 20 77 430 678 22
103 0.97297 0.01892 0.0041 0.0037 0.00328 31 20 77 430 678 22
104 0.98443 0.00685 0.00276 0.00328 31 21 77 430 678 24
105 0.0796 0.0079 0.0027 0.00328 0.0033 32 1 84 391 677 20
104 0.98443 0.00685 0.00276 0.00328 31 20 77 430 678 24
107 0.94143 0.00685 0.00276 0.00328 31 21 77 414 641 197
108 0.9901 0.007 0.0029 0.05001 0.003 33 21 84 391 677 20
109 0.98989 0.00729 0.0031 0.0520 0.00312 2 21 70 440 698 11
110 0.98734 0.00327 0.00312 0.0520 0.00313 22 21 70 440 684 196
111 0.9863 0.00284 0.00313 0.0554 0.00313 34 20 90 395 644 22
112 0.44767 0.00137 0.00284 0.04493 0.00313 32 2 83 427 690 22
114 0.97373 0.00284 0.00418 0.00316 39 32 98 34 385 605 23
112 0.94767 0.00737 0.00284 0.0448 0.00316 39 32 90 401 661 15
111 0.93642 0.00387 0.00328 0.00516 39 32 76 399 612 20
114 0.9737 0.00284 0.00458 0.00543 0.00406 31 22 76 399 612 20
114 0.9737 0.0046 0.00357 0.00281 0.04150 0.00313 23 21 77 382 606 22
115 0.7079 0.0028 0.00418 0.00297 33 22 4 78 380 659 25
115 0.94662 0.01075 0.00287 0.00457 0.00297 33 22 4 78 6380 659 25
115 0.94662 0.01075 0.00284 0.04158 0.002173 32 27 76 399
 | 91 0.98979 0.00737 0.00284 0.04212 0.00316 35 18 76 425 738 11
92 0.98468 0.01204 0.00328 0.04376 0.00328 32 0 92 413 667 2
93 0.93458 0.0113 0.00277 0.05135 0.00308 36 18 78 384 601 2
94 0.98648 0.01166 0.00286 0.05298 0.00318 30 25 81 386 568 2
95 0.98561 0.01178 0.00221 0.0533 0.00321 33 16 83 376 599 2
96 0.90561 0.0178 0.00221 0.0521 0.00313 32 19 76 336 823 2
98 0.9009 0.07207 0.0223 0.0221 0.0031 33 21 9 76 366 823 2
98 0.9009 0.07207 0.0270 0.0223 0.0221 0.00313 32 19 76 374 578 2
100 0.98462 0.0123 0.00317 0.0523 0.00321 0.0033 34 20 77 418 645 1
101 0.9867 0.00998 0.0333 0.05643 0.0033 31 122 87 431 673 2
103 0.97297 0.01892 0.0027 0.00278 0.05249 0.0033 31 22 97 4418 645 1
104 0.9772 0.0179 0.0027 0.00278 0.05249 0.0033 31 22 97 4418 645 1
105 0.9696 0.00729 0.00278 0.05249 0.0033 31 22 87 431 673 2
103 0.97297 0.01892 0.00814 0.08108 0.00811 31 17 70 425 860 12
105 0.7095 0.00799 0.0027 0.04497 0.003 29 22 92 419 654 11
10 0.98470 0.00895 0.00275 0.00375 0.00333 31 21 77 4418 641 17
Figure (9-f) Samples Used In Preparing and Testing the Prediction
Model.
108 0.9901 0.007 0.0029 0.00501 0.0033 32 21 84 391 677 22
109 0.98989 0.00729 0.0028 0.0521 0.0031 32 22 17 70 4416 641 17
110 0.9573 0.00320 0.00275 0.0033 30 22 22 92 449 654 11
111 0.9563 0.00726 0.00375 0.00333 32 12 77 4430 578 2
107 0.94145 0.00826 0.00276 0.00333 32 12 77 443 654 11
111 0.9563 0.00729 0.00281 0.0521 0.0031 32 21 70 4410 661 13
111 0.9563 0.00729 0.00281 0.0521 0.0031 32 22 90 401 661 13
113 0.95863 0.00729 0.00281 0.0521 0.0031 32 2 90 84 385 605 22
114 0.97377 0.00450 0.00799 0.0035 0.00541 0.0031 32 2 76 399 612 21
115 0.94767 0.00737 0.0028 0.00451 0.0031 36 20 84 427 690 21
116 0.95642 0.00370 0.00264 0.0391 3.0031 32 2 76 399 612 21
115 0.97079 0.00281 0.0051 0.0031 32 2 76 399 612 21
115 0.97079 0.00281 0.0051 0.0031 32 2 76 399 612 21
115 0.97079 0.00281 0.00264 0.0391 32 2 76 399 612 21
115 0.97079 0.00284 0.00361 0.00431 322 76 399 612 21
115 0.97079 0.00284 0.00264 0.03907 33 24 78 | 91 0.98979 0.00737 0.00284 0.04212 0.00316 35 18 76 425 738 1
92 0.98468 0.01204 0.00328 0.04376 0.00328 33 20 92 413 667 2
93 0.39458 0.0116 0.0028 0.0538 0.00318 30 25 81 386 586 2
94 0.98548 0.0116 0.0028 0.05298 0.00318 30 25 81 386 586 2
95 0.98501 0.01178 0.00321 0.0533 0.00321 33 15 83 376 589 2
96 0.70855 0.00729 0.00281 0.0521 0.00313 32 19 76 369 623 2
98 0.9009 0.0720 0.00282 0.6209 0.00313 32 19 76 369 623 2
98 0.9009 0.0720 0.00282 0.02013 0.0038 42 20 77 418 645 11
101 0.9867 0.00998 0.0033 0.05643 0.00333 31 22 87 431 673 2
102 0.6845 0.00278 0.00278 0.02269 0.00313 31 17 85 374 578 2
103 0.97297 0.01280 0.00278 0.00284 0.00333 31 22 87 431 673 2
103 0.97297 0.01892 0.0021 0.05319 0.0033 31 22 87 431 673 2
103 0.97297 0.01892 0.0021 0.00308 0.00211 31 17 70 425 650 1
104 0.97872 0.01702 0.00278 0.00278 0.00246 22 17 64 390 642 2
103 0.97297 0.01892 0.0027 0.00278 0.00284 31 20 77 418 645 11
106 0.98645 0.00296 0.00278 0.00234 31 21 77 414 641 17
Figure (9-f) Samples Used In Preparing and Testing the Prediction
Model.
108 0.9901 0.007 0.0029 0.0501 0.003 33 21 84 391 677 24
109 0.98445 0.00296 0.00310 0.0028 31 20 77 430 678 2
110 0.9574 0.00320 0.00214 0.00294 31 21 77 414 641 17
Figure (9-f) Samples Used In Preparing and Testing the Prediction
111 0.9867 0.0039 0.0021 0.0493 0.00313 32 9
12 90 401 661 11
111 0.93642 0.0138 0.00281 0.0031 32 22 17 6 399 612 2
114 0.9737 0.00280 0.00214 0.00294 33 21 70 410 668 11
111 0.93642 0.0138 0.00218 0.0524 0.00313 32 9
112 0.94763 0.00739 0.0028 0.00548 0.00313 32 9
114 0.9737 0.00280 0.00246 0.00313 32 9
114 0.9737 0.00280 0.00248 0.00313 32 9
114 0.9737 0.00280 0.00281 0.0463 0.00313 32 9
114 0.9737 0.00280 0.00281 0.0463 0.00313 32 29 90 401 661 11
110 0.95642 0.0138 0.00312 0.0520 0.00312 2 21 76 399 612 22
114 0.9733 0.00280 0.00281 0.0448 0.00313 32 29 0401 661 12
115 0.7179 0.0089 0.00267 0.0416 0.00321 32 21 8 84 386 500 22
114 0.9733 0.00280 0.00267 0.0414 0.00297 33 24 78 380 539 21
115 0.7174 0.00280 0.00267
 | 91 0.98979 0.00737 0.00224 0.04212 0.00316 35 18 76 425 738 11
92 0.98468 0.0120 0.00328 0.04376 0.00228 33 20 92 413 667 2
93 0.93458 0.0113 0.00277 0.0513 0.00308 36 18 78 384 601 2
94 0.98548 0.0116 0.00226 0.05298 0.00318 30 25 81 386 566 2
95 0.98501 0.01178 0.00221 0.0533 0.0021 33 15 83 376 599 2
96 0.70855 0.00729 0.00231 0.0521 0.00313 32 19 76 369 623 2
98 0.9009 0.07207 0.0270 0.0223 0.02703 36 22 82 400 602 1
99 0.98413 0.0127 0.00317 0.0523 0.00301 33 12 9 76 369 623 2
98 0.9009 0.07207 0.0270 0.0253 0.00521 0.00313 32 19 76 369 623 2
98 0.9009 0.07207 0.0270 0.0253 0.00521 0.00313 32 19 76 369 623 2
98 0.9042 0.0123 0.00317 0.0523 0.00308 34 20 77 418 645 11
10 0.9867 0.00998 0.0033 0.0563 0.0033 31 22 87 431 673 2
103 0.97297 0.01892 0.0017 0.0529 0.0033 31 22 87 431 673 2
104 0.9787 0.01892 0.00426 0.7092 0.00426 217 7 44 890 542 2
105 0.7095 0.00799 0.0027 0.04997 0.003 29 22 92 419 654 11
106 0.986012 0.00805 0.00228 0.04037 0.00308 31 20 77 418 644 11
116 0.98607 0.00998 0.0027 0.04997 0.003 29 22 92 419 654 11
105 0.98809 0.0072 0.0022 0.05001 0.0031 33 21 77 430 678 2
105 0.7095 0.00799 0.0027 0.04937 0.0030 29 22 92 419 654 11
106 0.986012 0.00807 0.00228 0.04037 0.00308 31 20 77 414 641 11
116 0.98607 0.00929 0.00228 0.04037 0.00308 31 20 77 430 678 2
104 0.9787 0.0032 0.00321 0.0523 0.00313 32 17 78 48 391 677 22
105 0.98609 0.0072 0.00228 0.00437 0.00337 32 21 70 4110 658 11
110 0.9573 0.0032 0.0032 0.0051 0.0031 33 21 77 382 606 22
111 0.9563 0.00729 0.0028 0.04378 0.00317 32 29 0401 661 11
113 0.95863 0.00729 0.0028 0.04478 0.00313 36 20 83 427 690 21
114 0.9737 0.0084 0.0438 0.00347 0.00237 32 377 382 606 22
115 0.70179 0.0089 0.0027 0.00281 0.0501 32 218 84 385 550 22
116 0.98602 0.0175 0.00284 0.0478 0.00313 36 20 83 427 690 21
116 0.98602 0.0175 0.00284 0.0478 0.00313 32 29 0 401 661 11
113 0.95863 0.00729 0.00281 0.0578 0.00313 32 29 0 401 661 11
113 0.95863 0.00729 0.00284 0.0478 0.00313 32 29 0 401 661 11
114 0.9737 0.0084 0.0478 0.00347 0.0029 | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | |
| 0.98468 0.01204 0.00328 0.00376 0.00328 33 20 92 413 657 0.93458 0.0113 0.0077 0.06135 0.00308 36 18 76 3346 661 0.98548 0.01166 0.00286 0.05298 0.00318 30 25 61 386 586 0.98548 0.01176 0.00720 0.00221 0.0531 32 23 81 400 702 0.98967 0.00720 0.00221 0.05210 0.00313 32 19 76 369 623 0.9096 0.00720 0.02703 0.2223 0.02703 36 22 82 400 602 0.98475 0.0170 0.05291 0.00333 31 22 87 431 673 0.98462 0.01274 0.05244 0.00303 31 22 87 431 673 0.98476 0.09989 0.00333 0.05244 0.00301 <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td> <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td> <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td> <td>92 0.88468 0.01204 0.00328 0.04376 0.00328 33 20 92 413 667 22 93 0.93458 0.0113 0.00277 0.05135 0.00308 36 18 78 384 601 22 94 0.86464 0.01168 0.00277 0.05135 0.00318 30 26 81 384 601 22 95 0.98661 0.01178 0.00221 0.05235 0.00313 32 23 81 400 702 11 96 0.98675 0.00729 0.00220 0.00313 32 19 76 366 623 2 99 0.99413 0.01727 0.02703 0.2523 0.00308 34 20 77 418 645 11 10 0.98462 0.01720 0.00270 0.0252 0.00317 36 17 85 374 678 21 10 0.98472 0.01702 0.06543 0.00333 31 22 87 413 677 22<td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td><td>92 0.98468 0.01204 0.00328 0.04376 0.00328 33 20 92 413 6677 2 93 0.93468 0.0113 0.00277 0.06135 0.00308 36 18 78 384 6011 2 94 0.99648 0.0116 0.00227 0.06135 0.00318 30 25 81 386 686 2 95 0.98605 0.00729 0.00221 0.00313 32 13 15 83 376 699 2 81 4000 702 1 97 0.98979 0.0729 0.00220 0.05231 0.0030 32 28 81 400 76 369 23 2 82 400 602 1 9 0.98413 0.0127 0.00313 0.5643 0.00333 31 22 87 431 673 2 10 0.9847 0.00276 0.06297 0.0033 31 2</td></td>
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 | 92 0.88468 0.01204 0.00328 0.04376 0.00328 33 20 92 413 667 22 93 0.93458 0.0113 0.00277 0.05135 0.00308 36 18 78 384 601 22 94 0.86464 0.01168 0.00277 0.05135 0.00318 30 26 81 384 601 22 95 0.98661 0.01178 0.00221 0.05235 0.00313 32 23 81 400 702 11 96 0.98675 0.00729 0.00220 0.00313 32 19 76 366 623 2 99 0.99413 0.01727 0.02703 0.2523 0.00308 34 20 77 418 645 11 10 0.98462 0.01720 0.00270 0.0252 0.00317 36 17 85 374 678 21 10 0.98472 0.01702 0.06543 0.00333 31 22 87 413 677 22 <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td> <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td> <td>$\begin{array}{cccccccccccccccccccccccccccccccccccc$</td> <td>92 0.98468 0.01204 0.00328 0.04376 0.00328 33 20 92 413 6677 2 93 0.93468 0.0113 0.00277 0.06135 0.00308 36 18 78 384 6011 2 94 0.99648 0.0116 0.00227 0.06135 0.00318 30 25 81 386 686 2 95 0.98605 0.00729 0.00221 0.00313 32 13 15 83 376 699 2 81 4000 702 1 97 0.98979 0.0729 0.00220 0.05231 0.0030 32 28 81 400 76 369 23 2 82 400 602 1 9 0.98413 0.0127 0.00313 0.5643 0.00333 31 22 87 431 673 2 10 0.9847 0.00276 0.06297 0.0033 31 2</td>
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| 0.93458 0.01166 0.00277 0.06135 0.00318 36 18 78 384 601 0.98548 0.01166 0.00286 0.05295 0.00318 30 25 81 386 586 0.98541 0.01176 0.00221 0.05513 0.00318 30 25 81 386 586 0.98657 0.00729 0.00221 0.0521 0.00313 32 23 81 400 702 0.98079 0.00729 0.00229 0.00209 0.00313 32 23 81 400 702 0.98042 0.01721 0.00317 0.0521 0.00313 31 22 82 400 602 0.98443 0.0127 0.00309 34 20 77 418 645 0.9847 0.09869 0.00333 0.06543 0.00309 34 20 77 418 645 0.98470 0.09869 0.00327 0.04262 217
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94 0.98564 0.0116 0.0026 0.05280 0.00318 30 25 81 386 586 2
95 0.98501 0.01178 0.00221 0.05353 0.00321 33 15 83 376 599 2
96 0.70855 0.00729 0.00281 0.0521 0.00313 32 13 81 400 772 1
97 0.98979 0.00729 0.00281 0.0521 0.00313 32 19 76 3869 623 2
98 0.9009 0.07207 0.02703 0.22523 0.02703 36 22 82 400 602 1
99 0.98462 0.01231 0.00317 0.05231 0.00318 34 20 77 418 645 1
10 0.98462 0.01231 0.00330 0.05631 0.00308 34 20 77 418 645 1
10 0.98462 0.01231 0.00330 0.05631 0.00308 34 25 80 372 580 2
103 0.97297 0.01790 0.00270 0.00278 0.05249 0.00313 31 22 87 431 673 2
104 0.97872 0.01790 0.00270 0.00426 0.7090 2.00462 21 17 64 380 642 2
105 0.7095 0.00729 0.00275 0.00327 0.00329 22 92 419 654 1
10 0.98645 0.00278 0.00278 0.00329 0.00242 31 21 77 418 654 1
10 0.98642 0.01702 0.00275 0.00497 0.003 29 22 92 419 654 1
10 0.98443 0.00585 0.00278 0.00324 0.00314 21 77 414 654 1
17 0.94143 0.00585 0.00278 0.00324 31 20 77 418 654 1
10 0.98692 0.00799 0.0027 0.00490 0.00242 31 21 77 414 654 1
17 0.94143 0.00585 0.00278 0.00331 20 22 92 419 654 1
10 0.98742 0.01702 0.00275 0.00497 0.003 29 22 92 419 6564 1
10 0.98991 0.007 0.0029 0.00270 0.00313 21 84 391 677 22
107 0.94143 0.00585 0.00284 0.04934 0.00342 31 21 77 414 641 1
10 0.95734 0.0032 0.00370 0.570 0.00331 32 1 84 391 677 22
109 0.98989 0.00729 0.00281 0.0521 0.00313 41 20 90 395 644 22
110 0.95734 0.0032 0.00370 0.0570 0.00331 22 77 410 698 11
11 0.9563 0.00729 0.00281 0.0553 0.00313 32 29 90 401 661 11
11 0.9563 0.00729 0.00281 0.0553 0.00313 32 29 90 401 661 12
11 0.95734 0.00832 0.00370 0.0573 0.00331 32 2 76 399 612 22
114 0.97337 0.0046 0.0036 0.0554 0.00313 32 18 84 385 655 22
117 0.9477 0.0028 0.00560 0.0031 32 28 84 385 550 22
118 0.7014 0.0089 0.00281 0.0418 0.00313 32 28 84 386 550 22
117 0.94427 0.01284 0.00289 0.0214 0.00321 32 18 84 385 550 22
118 0.70140 0.0089 0.00264 0.03061 0.00231 32 18 84 385 550 22
118 0.70140 0.0028 0.00264 0.03031 0.0224 83 439 678 11
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Model. 108 0.9901 0.007 0.0029 0.05001 0.003 33 21 84 391 677 22 109 0.98989 0.00729 0.00241 0.0051 0.00313 41 20 90 395 644 22 100 0.9574 0.00312 0.0520 0.00313 21 70 410 668 11 111 0.93642 0.0137 0.00347 0.0578 0.00347 30 20 84 385 605 22 111 0.94767 0.00737 0.00284 0.0418 0.00316 39 32 90 401 661 11 113 0.95683 0.00284 0.00316 39 32 90 401 661 12 21 114 0.97337 0.00284 0.00365 0.05543 0.00406 31 22 76 399 612 22</td><td>Figure (9-f) Samples Used In Preparing and Testing the Prediction Model. 108 0.9901 0.007 0.0029 0.05001 0.003 33 21 84 391 677 2 109 0.98909 0.0070 0.00281 0.0501 0.003 33 21 84 391 677 2 109 0.98999 0.0079 0.00281 0.05203 0.00313 41 20 90 395 644 22 110 0.95734 0.00381 0.05203 0.00313 32 21 70 410 698 11 111 0.95674 0.00387 0.00347 30 20 84 386 605 2 112 0.94767 0.00370 0.0024 0.04738 0.00316 33 20 84 386 606 2 114 0.97370 0.00246 0.00351 33 24 78 380 639 2</td></t<> | Figure (9-f) Samples Used In Preparing and Testing the Prediction Model. 108 0.9901 0.007 0.0029 0.05001 0.003 33 21 84 391 677 24 109 0.98989 0.00729 0.00281 0.0501 0.003 33 21 84 391 677 24 109 0.98989 0.00729 0.00281 0.0512 0.00313 21 70 410 698 111 0.93642 0.01337 0.0037 0.00284 0.0413 30 20 84 385 605 22 111 0.94767 0.00737 0.00284 0.04138 0.00316 39 32 90 401 661 111 13 0.95683 0.00729 0.00281 0.04168 0.00313 36 20 83 427 690 22 114 0.97307 0.00267 0.04513 0.00406 31 22 76 399 6
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 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 124 0.98573 0.011598 0.002609 0.048323 0.002899 36 18 75 466 776 11 Figure (9-g) Samples Used In Preparing and Testing the Prediction Model. 125 0.98256 0.0142 0.00296 0.0564 0.00228 30 19 80 396 622 2 126 0.98256 0.0142 0.00290 0.0567 0.00328 30 19 75 438 683 1 127 0.98437 0.0123 0.00326 0.05640 0.00328 26 25 75 428 629 1 128 0.64891 0.00366 0.05408 0.00311 30 22 78 376 582 2 130 0.9678 0.01111 0.00280 0.06582 0.0033 33 21 76 416 672 1 131 0.96878 0.01118 | | | | |
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 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 117 0.98427 0.01284 0.00289 0.0214 0.00321 32 18 84 385 550 22 118 0.70104 0.00394 0.07302 0.00438 31 23 82 387 596 20 119 0.98609 0.01196 0.00296 0.05478 0.00329 22 28 84 439 678 18 120 0.98648 0.01166 0.00286
 0.00318 32 17 70 314 656 22 121 0.98693 0.01136 0.00277 0.05136 0.00308 32 21 83 421 653 18 120 0.98573 0.01159 0.00386 0.00289 0.01038 24 24 81 396 652 21 124 0.98573 0.01159 0.00269 0.04323 0.00289 36 18 75 466 776 15 igure (9-g) Samples Used In Preparing and Testing the Prediction 125 <t< td=""><td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td></t<> | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$
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 0.00286 0.06478 0.00318 32 17 70 314 653 18 121 0.98653 0.01196 0.00277 0.0515 0.00385 0.00299 31 16 90 409 636 21 123 0.98052 0.0169 0.00386 0.00289 36 18 75 466 776 16 Note: Note: <td <="" colspan="4" td=""><td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td><td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td><td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td><td>124 0.986793 0.011598 0.002609 0.048323 0.002899 36 18 75 466 776 11 Figure (9-g) Samples Used In Preparing and Testing the Prediction L25 0.98276 0.0142 0.00295 0.0564 0.00238 30 19 80 396 622 2 126 0.98276 0.0123 0.00320 0.00328 30 19 75 438 683 1 127 0.98476 0.0123 0.00326 0.0566 0.00260 372 10 75 428 629 1 128 0.64891 0.00369 0.6036 0.222 78 376 582 2 130 0.9768 0.01111 0.00280 0.04879 0.00233 34 24 75 380 638 2 131 0.9768 0.01114 0.00280 0.06582 0.00333 33 21 76</td></td> | <td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td> <td>$\begin{array}{c c c c c c c c c c c c c c c c c c c$</td> <td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td> <td>$\begin{array}{c ccccccccccccccccccccccccccccccccccc$</td> <td>124 0.986793 0.011598 0.002609 0.048323 0.002899 36 18 75 466 776 11 Figure (9-g) Samples Used In Preparing and Testing the Prediction L25 0.98276 0.0142 0.00295 0.0564 0.00238 30 19 80 396 622 2 126 0.98276 0.0123 0.00320 0.00328 30 19 75 438 683 1 127 0.98476 0.0123 0.00326 0.0566 0.00260 372 10 75 428 629 1 128 0.64891 0.00369 0.6036 0.222 78 376 582 2 130 0.9768 0.01111 0.00280 0.04879 0.00233 34 24 75 380 638 2 131 0.9768 0.01114 0.00280 0.06582 0.00333 33 21 76</td>
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 | | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | 124 0.986793 0.011598 0.002609 0.048323 0.002899 36 18 75 466 776 11 Figure (9-g) Samples Used In Preparing and Testing the Prediction L25 0.98276 0.0142 0.00295 0.0564 0.00238 30 19 80 396 622 2 126 0.98276 0.0123 0.00320 0.00328 30 19 75 438 683 1 127 0.98476 0.0123 0.00326 0.0566 0.00260 372 10 75 428 629 1 128 0.64891 0.00369 0.6036 0.222 78 376 582 2 130 0.9768 0.01111 0.00280 0.04879 0.00233 34 24 75 380 638 2 131 0.9768 0.01114 0.00280 0.06582 0.00333 33 21 76 |
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 0.0518 0.00318 32 11 630 421 683 18 121 0.98593 0.01130 0.00277 0.05136 0.00388 0.00299 31 16 50 4499 636 21 122 0.98593 0.01159 0.00380 0.06825 0.00398 24 24 81 398 658 21 124 0.98573 0.01159 0.00269 0.48323 0.00289 36 18 75 466 76 15 Figure (9-g) Samples Used In Preparing and Testing the Predictio 127 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$
 | $ \begin{array}{c c c c c c c c c c c c c c c c c c c $ | 122 0.72731 0.01096 0.00289 0.03985 0.00299 31 16 90 409 636 22 123 0.98052 0.0158 0.00269 0.04823 0.00289 31 16 90 409 636 22 123 0.98052 0.0158 0.00289 0.00289 36 18 76 466 776 11 Vigure (9-g) Samples Used In Preparing and Testing the Predictio Model. 0.98275 0.0142 0.00298 0.05627 0.00332 37 20 75 438 683 1 128 0.98375 0.0142 0.00298 0.05527 0.00332 37 20 75 438 683 1 128 0.4847 0.0126 0.00382 0.0368 0.00313 22 100 374 633 2 100 374 633 2 130 0.7142 0.01111 0.0028 0.06188 0.00333
 | 123 0.98052 0.0159 0.00358 0.06625 0.00398 24 24 81 398 658 22 124 0.98079 0.01159 0.00269 0.048323 0.00299 36 18 75 466 776 11 Figure (9-g) Samples Used In Preparing and Testing the Predictio Model. 125 0.98285 0.0142 0.00296 0.05627 0.0032 30 19 80 396 622 2 126 0.98285 0.0142 0.00286 0.06527 0.0032 37 20 75 438 663 1 127 0.98470 0.0126 0.06486 0.00466 34 22 100 374 653 2 128 0.64891 0.00466 0.00283 0.4849 0.00211 30 22 78 376 582 2 120 0.7124 0.01117 0.0028 0.0618 0.00313 32 1 76 438 648 1 130 0.98768 0.011 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$ | | | | |
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 | | 116 0.98662 0.01075 0.00264 0.03907 0.00293 33 24 78 380 539
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Figure (9-i) Samples Used In Preparing and Testing the Prediction

nical Specifications of Industrial Products...

Azouza & Naser

se c	of Mul	tiple l	Linea	Regr	ression	Tech	nolog	gy in (Control	ling th	ne Te
144	0.99039	0.00693	0.00267	0.0416	0.00297	31	20	76	409	635	19
145	0.98989	0.00729	0.00281	0.04168	0.00313	31	20	74	355	561	22
146	0.98989	0.00729	0.00281	0.04481	0.00313	30	21	82	435	688	20
147	0.67518	0.01039	0.0028	0.06232	0.00312	33	19	73	381	663	20
148	0.98267	0.01251	0.00482	0.07147	0.00536	31	21	88	392	635	20
149	0.98614	0.01	0.00386	0.05717	0.00429	29	21	81	403	617	19
150	0.98845	0.00834		0.05955	0.00357	36	20	114	386	595	25
151	0.97787	0.01716	0.00463	0.06862	0.00515	31	21	82	393	529	20
152	0.98746	0.00987	0.00267	0.0395	0.00296	32	27	72	390	607	27
153	0.9901	0.00715	0.00276	0.05104	0.00306	34	24	74	405	624	24
154	0.9891	0.00713	0.00270	0.0562	0.00300	32	24	72	394	614	24
155	0.70479	0.00796	0.00307	0.01819	0.00341	33	23	82	431	670	18
156	0.75556	0.00790	0.00307	0.01703	0.00341	34	16	82	431	686	20
157	0.5735	0.00745	0.00287	0.05482	0.00253	30	22	76	374		20
157							19			602	
	0.98501	0.01204	0.00296	0.06129	0.00328	31		77	381	603	20
159	0.95664	0.00936	0.00281	0.04159	0.00312	29	22	81	432	642	18
160	0.761118				0.003262	34	23	86	461	743	17
161	0.309634	0.008336	0.003215	0.053591	0	32	19	23	409	643	20
162	0.98517	0.01191	0.00292	0.06496	Moc 0.00325	del. 30	22	92	362	581	22
163	0.66688	0.00753	0.0029	0.05378	0.00323	29	18	87	394	627	23
164	0.60024	0.00934	0.0036	0.04402	0.004	24	17	76	400	615	19
165	0.85885	0.00707	0.00273	0.04042	0.00303	30	22	75	430	686	18
166	0.96905	0.00729	0.00281	0.04168	0.00313	37	23	75	438	667	19
167	0.96771	0.00761	0.00294	0.04349	0.00326	32	25	79	468	755	16
168	0.93677	0.00701	0.06323	0.23419	0.07026	32	15	80	479	717	15
169	0.98787	0.00875	0.00338	0.06252	0.00375	29	20	77	456	778	17
170	0.9903	0.007	0.0027	0.03601	0.003	34	23	71	417	687	19
171	0.9891	0.00787	0.00303	0.03934	0.00337	27	19	72	410	663	19
172	0.98934	0.00769	0.00297	0.04397	0.0033	26	22	75	455	707	17
173	0.73551	0.00686	0.00265	0.03923	0.00294	28	23	72	513	778	16
174	0.97761	0.00796	0.00307	0.04547	0.00341	33	24	77	462	666	16
175	0.9901	0.00715	0.00276	0.05104	0.00306	30	21	73	459	698	17
176	0.98979	0.00722	0.00278	0.05155	0.00309	32	23	73	433	656	20
177	0.986	0.01	0.004	0.05716	0.00429	28	17	68	420	691	20
178	0.988602	0.008141	0.003257	0.046522	0.003489	30	17	74	448	697	17
179	0.97914	0.0149	0.00596	0.085143	0.006386	28	19	92	364	553	22
Fig	ure (9					parir			ng the p	redict	ion
180	0.98383	0.01167	0.0045	0.0667	0.005	34	20	82	419	634	19
181	0.98934	0.00769	0.00297	0.05496	0.0033	32	20	73	397	681	22
182	0.99069	0.00788	0.00143	0.05629	0.00338	23	18	64	479	762	17
183	0.6462	0.01346	0.00377	0.05385	0.00404	34	15	103	374	639	22
184	0.97349	0.02071	0.0058	0.06214	0.00621	32	23	97	425	661	19
185	0.98698	0.01018	0.00285	0.0407	0.00305	29	20	83	426	660	19
186	0.9901	0.00715	0.00276	0.04083	0.00306	24	17	80	414	673	21
187	0.43538	0.00956	0.00270	0.06371	0.00319	29	14	82	435	706	18
188	0.79581	0.01007	0.00272	0.04029	0.00302	29	21	76	443	747	18
189	0.66698	0.01112	0.00429	0.06352	0.00476	33	27	83	433	727	17
190	0.93306	0.00976	0.00293	0.0434	0.00325	39	21	87	433	672	19
191	0.77837	0.00841	0.00293	0.0434	0.00325	30	17	73	423	605	19
192	0.98979	0.00737	0.00284	0.04207	0.00316	33	20	77	402	726	18
192	0.98968	0.00737	0.00284	0.04212	0.00310	30	20	81	433	606	10
193	0.98968	0.00745	0.00287	0.04257	0.00319	30	24	72	444 437	703	17
194	0.98796	0.00926	0.00278	0.04116	0.00309	30	17	82	437	703	18
195	0.7475		0.00297	0.04397	0.0033	30	27	82	448 378	610	21
	0		0.010011	0.185391		31 28		88 81			
	0				0.309278	30	19		337	534	23 18
197		0.031002	0.012289	0.22/083	0.013000		16	76	433	787	
198) (1 •	•		1	ng the j	1.	. •

3.1. Forecasting Models:

To use the prediction equation for multiple linear regression analysis, it is necessary to know whether the independent variables have an effect on the dependent variable or not, and for this we calculated the correlation rate R, which shows if there is a relationship between the independent variables and the successive variable.

3.1.1. Yield Effort Prediction Model:

After confirming the existence of a correlation, we can use the prediction equation to analyze the multiple linear regression, and Figure (10) shows the results of the multiple linear regression analysis and the statistical analysis of the yield effort prediction model.

SUMMARY OUTPI	JT							
Regression Statis	tics							
Multiple R	0.571961474							
R Square	0.327139928							
Adjusted R Squ	0.164022335							
Standard Erro	28.44561608							
Observations	42	_						
ANOVA								
	df	SS	MS	F	Significance F	1		
Regression	8	12982.35331	1622.794164	2.00554656	0.076770244			
Residual	33	26702.05145	809.1530742					
Total	41	39684.40476						
	Coefficients	Standard Error	t Stat	P-value	Lower 95%	Upper 95%	Lower 99.0%	Upper 99.0
Intercept	413.0300401	97.59253102	4.232189039	0.000173268	214.4765428	611.583537	146.2826546	679.77742
DRI	-38.68576338	39.88987724	-0.969814049	0.339194071	-119.8423288	42.4708021	-147.7158331	70.344306
FeMn	-4000.538448	2339.779756	-1.709792743	0.096692853	-8760.856155	759.779259	-10395.8038	2394.7269
FeSi	8428.08049	4766.385483	1.768233082	0.08626677	-1269.203688	18125.3647	-4599.769618	21455.930
Lime	-151.801289	308.5587445	-0.491968845	0.625998264	-779.5687749	475.966197	-995.1776982	691.57512
Dol.	434.4523967	4617.001681	0.094098384	0.925600033	-8958.908152	9827.81295	-12185.09046	13053.995
C	-0.933405579	1.390097842	-0.671467541	0.506596284	-3.761580904	1.89476975	-4.732927542	2.8661163
Si	3.31249016	1.397465834	2.370355024	0.023768047	0.469324544	6.15565578	-0.507170562	7.1321508
Mn	0.07144496	0.699204222	0.102180391	0.919231873	-1.351096725	1.49398665	-1.839673607	1.9825635

Figure (10) Results of the multiple linear regression analysis with the yield stress prediction model

Through Figure (11), it is necessary to know whether there is a relationship between the independent variables (chemicals) and the dependent variable (submission stress), by means of the correlation coefficient R where its value was 0.57 and this confirms the existence of a strong correlation between the independent variables and the dependent variable, while R2 The coefficient of determination indicates the influence of the independent variables on the dependent variable, where its value was 0.32, and this indicates the strength of

the effect. As for Adjusted (R2), the corrected coefficient of determination is the same as R2, but they differ from each other that Adjusted (R2) increases only when adding an independent variable that has an effect on the dependent variable and after knowing that there is a relationship, we test the hypothesis by tabular F test where if F The tabular F selects the null hypothesis H0: there is no relationship between the independent variables and the dependent variable. And if the tabular F > F selects the hypothesis H1: there is at least one relationship between the independent variables and the dependent variable, and this test is considered a comprehensive test, so we conduct another test to find out which of the independent variables have an effect on the dependent variable individually by T and P test -Value, where if the value of T > 2, then this independent variable has an effect on the dependent variable, and if T < 2, then this variable has no effect, and as for the P-Value test, if P-Value > 0.05, this variable has no effect on the dependent variable However, if P-Value < 0.05, this independent variable has an effect on the dependent variable.

3.1.2. Results of the Yield Effort Prediction Model:

These results are 42 samples obtained from the yield stress prediction model and were compared with the real stress as shown in Figure (11), where it was found that the mean error is close to zero. RESIDUAL OUTPUT

Observation	Predicted Yield Effort	Residuals	Standard Residuals	Percentile	Yield Effor
1	416.2195936	31.78040638	1.245314545	1.19047619	343
2	404.5664133	24.4335867	0.957429573	3.571428571	358
3	420.3287639	10.67123606	0.418152157	5.952380952	365
4	409.9324544	40.06754556	1.570045916	8.333333333	370
5	413.9422218	61.05777818	2.392547733	10.71428571	370
6	405.2354826	-21.23548256	-0.83211193	13.0952381	371
7	402.2449036	9.75509642	0.382253245	15.47619048	374
8	451.7519345	5.248065488	0.205645334	17.85714286	376
9	409.6985878	-27.69858777	-1.08536857	20.23809524	379
10	418.1207323	33.87926768	1.32755838	22.61904762	380
11	426.1674171	1.832582887	0.071809721	25	382
12	434.0828911	7.917108946	0.310231745	27.38095238	384
13	424.3704952	-5.370495164	-0.210442738	29.76190476	387
14	398.2020512	43.79794878	1.716221687	32.14285714	388
15	437.2076277	6.79237233	0.266158965	34.52380952	393
16	413.5710005	-19.57100052	-0.766889237	36.9047619	394
17	409.0179048	-39.01790483	-1.528915766	39.28571429	394
18	404.7516705	7.248329539	0.284025638	41.66666667	399
18	404.7516705	7.248329539	0.284025638	41.66666667	35

Figure (11-a) results of the yield stress prediction model and its

comparison with the real stress.

RESIDUAL OUT	TPUT			PROBABILITY OUTPUT	
Observation	Predicted (Yield Et	fort Residuals	Standard Residuals	Percentile	Yield Effo
19	415.9733639	-7.973363917	-0.312436095	44.04761905	401
20	419.1758176	-1.175817582	-0.046074387	46.42857143	403
21	415.5577758	21.44222422	0.840213098	48.80952381	406
22	416.7019989	-22.70199889	-0.889577341	51.19047619	408
23	423.6505009	9.349499107	0.366359923	53.57142857	409
24	408.822292	-34.82229201	-1.364510768	55.95238095	410
25	421.4346299	-11.43462993	-0.448065729	58.33333333	412
26	383.049877	3.950122953	0.154785483	60.71428571	412
27	386.6047265	-7.604726501	-0.297991045	63.0952381	418
28	401.831541	-31.83154104	-1.247318255	65.47619048	419
29	408.4935568	-20.49355675	-0.803039583	67.85714286	428
30	418.4670446	-38.46704464	-1.507330322	70.23809524	429
31	380.8169657	-15.81696566	-0.619787461	72.61904762	431
32	404.3840122	-1.384012244	-0.05423249	75	433
33	401.8155363	-2.815536324	-0.110326731	77.38095238	437
34	381.1411868	27.85881318	1.091646999	79.76190476	442
35	394.0055618	-18.00556185	-0.705547556	82.14285714	442
36	403.1300403	-45.13004032	-1.768419665	84.52380952	444
auro (1	1 h) rocul	ts of the	wield stress r	radiction mode	and

Figure (11-b) results of the yield stress prediction model and its comparison with the real stress.

PROBABILITY OUTPUT

			PROBABILITY OUTPUT	
ted (Yield Effort	Residuals	Standard Residuals	Percentile	Yield Effor
1.7134167	19.28658325	0.755744353	86.9047619	444
9.7644283	14.23557167	0.557820572	89.28571429	448
5.1874333	-52.1874333	-2.044963458	91.66666667	450
9.5373217	23.46267825	0.919384546	94.04761905	452
1.2762463	-0.27624633	-0.010824707	96.42857143	457
5.0525795	20.94742053	0.820824226	98.80952381	475
al Error	-3.41061E-12			
17117	-8.12049E-14			
	ted fyield Effort 1.7134167 9.7644283 6.1874333 9.5373217 1.2762463 5.0525795 al Error 17117	1.7134167 19.28658325 9.7644283 14.23557167 6.1874333 -52.1874333 9.5373217 23.46267825 1.2762463 -0.27624633 5.0525795 20.94742053	1.7134167 19.28658325 0.755744353 9.7644283 14.23557167 0.557820572 5.1874333 -52.1874333 -2.044963458 9.5373217 23.46267825 0.919384546 1.2762463 -0.27624633 -0.010824707 5.0525795 20.94742053 0.820824226	Effort Residuals Standard Residuals Percentile 11.7134167 19.28658325 0.755744353 86.9047619 9.7644283 14.23557167 0.557820572 89.28571429 5.1874333 -52.1874333 -2.044983458 91.66666667 9.5373217 23.46267825 0.919384546 94.04761905 1.2762463 -0.27624633 -0.010824707 96.42857143 5.0525795 20.94742053 0.820824226 98.80952381

Average Stepping Effort of The Sample = 407, 547619

Figure (11-c) results of the yield stress prediction model and its comparison with the real stress.

Through Figure (11), after performing the prediction process for 42

RESIDUAL OUTPUT

RESIDUAL OUTPUT

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samples, the total prediction for the yield effort was 17117, and the average error was -8.12049E-14, which is very close to zero, which indicates the accuracy of the prediction. As for the negative sign, this indicates that the prediction is greater than the real one. We subtract this value from all predictions until we get an average error equal to zero, and the average error is the result of subtracting the prediction from the real one, adding all the values of the subtraction process and dividing it by the number of samples (42 samples). Prediction was performed for only 42 samples because Microsoft Office Excel did not accept more than this size.

3.1.3. Tensile Strength Prediction Model:

After confirming the existence of a correlation, we can use the prediction equation to analyze the multiple linear regression, and Figure (12) shows the results of the multiple linear regression analysis of the tensile strength prediction model.

SUMMARY OUTPUT								
Regression Statistics								
Multiple R	0.997128759							
R Square	0.994265762							
Adjusted R Square	0.963673418							
Standard Error	54 22239823							
Observations	42							
ANOVA								
	df	SS	MS	F	ignificance F			
Regression	8	17332575.67	2166571.959	736.9120758	6.57E-35			
Residual	34	99962.32797	2940.06847					
Total	42	17432538	Contra Processo					
	Coefficients	Standard Error	t Stat	P-value	Lower 95%	Upper 95%	ower 99.05	Ipper 99.0%
Intercept	0	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A
DRI	64.0203302	63.82620404	1.003041481	0.3229264	-65.69012	193.7307829	-110.123	238.1634
FeMn	-2212.043288	3952.269399	-0.5596894	0.579360193	-10244.02	5819.934498	-12995.4	8571.306
FeSi	6357.878607	8495.264275	0.748402687	0.459363378	-10906.58	23622.33279	-16820.6	29536.31
Lime	-119.6940869	584.7570177	-0.204690296	0.839034554	-1308.063	1068.675152	-1715.14	1475.754
Dol.	-1232.957154	8756.876433	-0.140798738	0.888859825	-19029.07	16563.1569	-25125.2	22659.26
C	4.216962061	2.289888732	1.841557628	0.074277936	-0.436652	8.870575864	-2.03076	10.46468
Si	10.05367571	2.294171246	4.382269079	0.00010691	5.391359	14.71599263	3.794272	16.31308
Mn	3.469175392	0.920950068	3.766952749	0.000628095	1.59758	5.340771111	0.95646	5.98189

Figure (12) results of the multiple linear regression analysis of the tensile strength prediction model.

Through the results, it must be known whether there is a relationship between the independent variables (chemicals) and the dependent variable (tensile strength), through the correlation coefficient R, where its value was 0.997, and this confirms the existence of a strong correlation between the independent variables and the dependent variable. As for the R2 coefficient of determination, it indicates the effect of the independent variables on the dependent variable, where its value was 0.0994, and this indicates the strength of the effect, and the Adjusted (R2) coefficient of determination is the same as the meaning of R2, but they differ from each other that Adjusted (R2) increases only when adding an independent variable It has an effect on the dependent variable and after knowing that there is a relationship, we test the hypothesis by using the F tabular test where if F < F tabular selects the null hypothesis H0: there is no relationship between the independent variables and the dependent variable. And if the tabular F > F selects the hypothesis H1: there is at least one relationship between the independent variables and the dependent variable, and this test is considered a comprehensive test, so we conduct another test to find out which of the independent variables have an effect on the dependent variable individually by T and P test -Value, where if the value of T > 2, then this independent variable has an effect on the dependent variable, but if T < 2, then this variable has no effect, and as for the P-Value test, if P-Value > 0.05, this variable has no effect on the dependent variable. If the P-Value < 0.05, this independent variable has an effect on the dependent variable.

3.1.4. Results of the Tensile Strength Prediction Model:

These results are 42 samples obtained from the tensile strength prediction model and were compared to the real tensile strength as shown in Figure (13), where it was found that the mean error is close to zero.

SIDUAL OUTPUT			
Observation	قرة الشد Predicted	Residuals	Standard Residuals
1	708.1988264	38.80117357	0.795337254
2	634.0081868	33.99181317	0.696756125
3	619.9045078	61.09549221	1.252320911
4	640.8586352	32.14136484	0.658826074
5	650.5047386	120.4952614	2.469883294
6	645.6264589	-26.62645891	-0.545782841
7	631.4085979	21.59140206	0.442575439
8	686.913766	13.08623401	0.268238521
9	656.3976541	-73.39765409	-1.504487708
10	677.5308601	54.46913993	1.116495513
11	663.3158914	28.68410864	0.587960057
12	693.9831872	23.01681284	0.471793171
13	703.6638175	-53.66381748	-1.099988205
14	638.1818323	73.81816773	1.513107297
15	681.6208495	47.37915054	0.971166592
16	675.1227637	-24.12276372	-0.49446269
17	659.4309267	-46.43092666	-0.951730124
18	610.3628864	11.63711355	0.238534794
19	649.7066605	23.29333951	0.477461349
20	658.5194648	-5.519464804	-0.113136681

Figure (13-a) Results of the tensile strength prediction model and their comparison with the real tensile strength.

Observation	قوة الشد Predicted	Residuals	Standard Residuals
21	662.6081195	34.39188054	0.704956612
22	639.4265376	-0.426537592	-0.008743066
23	660.7476296	-5.747629617	-0.117813549
24	656.5640492	-92.56404919	-1.897355929
25	716.7018275	-58.70182751	-1.20325614
26	560.2204891	34.77951092	0.712902167
27	609.4748475	-16.4748475	-0.337697517
28	609.7101182	-55.71011821	-1.141932792
29	668.3872533	-59.38725332	-1.217305835
30	703.0552519	-77.05525189	-1.57946028
31	500.2729844	45.72701557	0.937301521
32	647.7709228	3.229077211	0.066188859
33	636.8178465	-39.81784651	-0.816176775
34	603.0751032	72.92489683	1.494797242
35	636.5196068	-28.51960678	-0.584588137

Figure (13-b) Results of the tensile strength prediction model and their comparison with the real tensile strength.

Observation	قوة الشد Predicted	Residuals	Standard Residuals
36	662.8197844	-103.8197844	-2.128073321
37	643.6364033	-10.63640333	-0.218022473
38	593.1373675	33.86263247	0.69410821
39	578.3803834	41.38038338	-0.848205286
40	580.9595089	-7.959508881	-0.163152126
41	545.2677191	10.73228094	0.21998775
42	616.2162295	43.78377048	0.897469344
	Total Error =	34.96950514	
	Average Error =	0.832607265	
	26917.03049		

Figure (13-c) Results of the tensile strength prediction model and their comparison with the real tensile strength.

In Figure (13), after performing the prediction process for 42 samples, the average error was 0.832, which is very close to zero, which indicates the accuracy of the prediction.

3.1.5. Elongation Ratio Prediction Model:

After confirming that there is a correlation, we can use the prediction equation to analyze the multiple linear regression, and Figure (14) shows the results of the multiple linear regression analysis and the statistical analysis of the elongation ratio prediction model.

Use of Multiple Linear Regression Technology in Controlling the Technical Specifications of Industrial Products...

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SUMMARY OUTPUT								
Regression Statistics								
Multiple R	0.990863478							
R Square	0.981810431							
Adjusted R Square	0.948653755							
Standard Error	3.049099815							
Observations	42	_						
ANOVA								
	df	SS	MS	F	Significance F			
Regression	8	17061.9017	2132.737709	229.400397	1.19452E-26			
Residual	34	316.098329	9.297009684					
Total	42	17378						
	Coefficients	itandard Erro	t Stat	P-value	Lower 95%	Jpper 95%	ower 99.0	Upper 99.0%
Intercept	0	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A	#N/A
DRI	5.900916963	3.5891527	1.644097495	0.10937265	-1.393118903	13.195	-3.89171	15.693541
FeMn	592.145152	222.248818	2.664334318	0.01170958	140.4812126	1043.81	-14.2373	1198.52757
FeSi	-1194.12097	477.716028	-2.499646022	0.01742108	-2164.956746	-223.285	-2497.52	109.276751
Lime	30.94194816	32.8827675	0.940977616	0.35335428	-35.88387556	97.7678	-58.7752	120.659106
Dol.	-318.9235379	492.427321	-0.647656058	0.52155702	-1319.656258	681.809	-1662.46	1024.61239
C	0.173799475	0.12876781	1.349712161	0.18602689	-0.087888194	0.43549	-0.17753	0.52512883
Si	0.000371942	0.12900863	0.002883079	0.99771649	-0.261805131	0.26255	-0.35161	0.35235835
Mn	0.10268001	0.05178798	1.982699512	0.05552774	-0.002565836	0.20793	-0.03862	0.24397805

Figure (14) results of the multiple linear regression analysis of the elongation ratio prediction model.

Through the results, it must be known whether there is a relationship between the independent variables (chemicals) and the dependent variable (elongation ratio), by means of the correlation coefficient R whose value was 0.998 and this confirms the existence of a strong correlation between the independent variables and the dependent variable, while R2 The coefficient of determination indicates the effect of the independent variables on the dependent variable, where its value was 0.981, and this indicates the strength of the effect. As for Adjusted (R2), the corrected coefficient of determination is the same as R2, but they differ from each other that Adjusted (R2) increases only when adding an independent variable that has an effect on the dependent variable and after knowing that there is a relationship, we test the hypothesis by tabular F test where if F The tabular F selects the null hypothesis H0: there is no relationship between the independent variables and the dependent variable. If the tabular F > F selects the hypothesis H1: there is at least one relationship between the independent variables and the dependent variable, and this test is considered a comprehensive test, so we conduct another test to find out which of the independent variables have an effect on the dependent variable individually by T and P test -Value, where if the value of T > 2, then this independent variable has an effect on the dependent variable, but if T < 2, then this variable has no effect, and as for the P-Value test, if P-Value > 0.05, this variable has no effect on the dependent variable, If the P-Value < 0.05, this independent variable has an effect on the dependent variable.

3.1.6. Results of the Elongation Ratio Prediction Model:

These results are 42 samples obtained from the equation for predicting the elongation ratio and were compared with the true relative elongation ratio as shown in Figure (15), where it was found that the mean error is close to zero.

Observation	%لاستطالة Predicted	Residuals	Standard Residuals
1	21.0726868	-1.072686796	-0.391008753
2	20.10764223	-3.10764223	-1.132777357
3	18.00718119	-0.007181194	-0.002617642
4	19.73806845	1.261931554	0.459991011
5	19.84661656	-4.846616564	-1.766656873
6	20.41210911	-0.412109111	-0.150219309
7	20.11550498	-1.115504977	-0.406616556
8	16.75249696	-0.752496962	-0.274295256
9	21.2423502	4.757649798	1.734227291
10	20.44155049	-4.441550493	-1.619004846
11	18.87059557	-1.870595574	-0.681857226
12	18.98196027	1.018039727	0.371089162
13	20.21238904	-1.212389043	-0.4419321
14	20.58348869	1.416511307	0.516337408
15	18.06562174	-1.065621742	-0.388433446
16	20.51422383	-0.514223827	-0.187441496
17	20.43073524	0.569264758	0.207504655
18	19.12450461	1.875495386	0.683643274
19	19.38161619	5.618383813	2.047976407
20	18.76762279	-0.767622793	-0.279808824

Figure (15-a) results of the prediction model for the elongation rate and its comparison with the real elongation rate.

Observation	Predicted 21%	Residuals	Standard Residuals
21	19.21726595	-2.217265954	-0.808223239
22	18.44029118	1.559708821	0.568534827
23	18.98059515	7.01940485	2.558667404
24	20.00962497	0.99037503	0.361005008
25	20.52592265	-0.525922648	-0.191705873
26	20.62189811	1.378101893	0.502336661
27	21.03074562	-0.03074562	-0.011207192
28	19.80448282	6.195517177	2.258349274
29	20.4752151	-0.475215105	-0.173222292
30	20.55082091	-0.550820905	-0.200781623
31	18.32579155	5.674208448	2.068325236
32	20.58329295	-1.58329295	-0.577131559
33	20.65331924	-2.653319236	-0.96717052
34	21.28841077	-5.288410766	-1.927696797
35	22.01564244	-1.015642442	-0.37021532
36	20.86484841	1.135151587	0.413778009
37	21.69275521	-0.692755207	-0.252518583
38	16.70872873	-0.70872873	-0.258341147
39	20.12662535	2.873374647	1.047383675
40	24.28867697	-0.288676972	-0.105226636
41	23.55087287	-1.550872872	-0.565314004
42	21.82946211	-2.829462109	-1.031376965
	Total Error =	1.745745974	-
	Average Error =	0.04156538	
	844.254254		

Figure (15-b) results of the prediction model for the elongation rate and its comparison with the real elongation rate.

In Figure (15), after performing the prediction process for 42 samples, the mean error was 0.041, which is very close to zero, which indicates the accuracy of the prediction.

3.2. Testing the Yield Effort Prediction Model:

Testing the prediction model and calculating the mean error in predicting yield stress, and these results are shown in Figure (16) for all 198 samples obtained from the prediction model.

NO	DRI	FeMn	FeSi	Lime	Dol.	С	Si	Mn	Yield	Tensile		Expected Yie	Error
1	0.93647	0.00745	0.00287	0.04363	0.00319	34	23	81	Effort 448	Strength 747	20	Effort 416.2195936	31,78041
2	0.93779		0.00281	0.04897	0.00313	31	19	75	429	668	17	404.5664133	24.43359
3	0.66688	0.00729	0.00281	0.04168	0.00313	30	20	74	431	681	18	420.3287639	10.67124
4	0.93579	0.00753	0.0029	0.0484	0.00323	32	21	70	450	673	21	409.9324544	40.06755
5	0.95863	0.00729		0.0521	0.00313	30	22	72	475	771	15	413.9422218	61.05778
6	0.9244	0.00886		0.05065	0.0038	30	19	80	384	619	20	405.2354826	-21.23548
7	0.93579	0.00753	0.0029	0.04302	0.00323	31	18	77	412	653	19	402.2449036	9.755096
8	0.59473			0.08496	0	29	22	76	457	700	16	451.7519345	5.248065
9	0.84966	0.00959	0.0037	0.05482	0	32	21	75	382	583	26	409.6985878	-27.69859
10	0.9289	0.00834		0.05955	0.00357	29	23	79	452	732	16	418.1207323	33.87927
11	0.75023	0.007	0.0027	0.05002	0.003	33	24	70	428	692	17	426,1674171	1.832583
12	0.8651	0.00631		0.03514	0.0027	30	26	74	442	717	20	434.0828911	7.917109
13	0.94875	0.00722	0.00278	0.04125	0.00309	32	25	76	419	650	19	424.3704952	-5.370495
14	0.94087	0.00693	0.00267	0.04457	0.00297	35	18	74	442	712	22	398,2020512	43.79795
15	0.69409	0.00715	0.00276	0.0347	0.00306	33	26	70	444	729	17	437.2076277	6.792372
16	0.9329	0.00787	0.00303	0.0562	0.00337	34	23	72	394	651	20	413,5710005	-19.571
17	0.8904	0.00769	0.00297	0.05496	0.0033	34	21	74	370	613	21	409.0179048	-39.0179
18	0.8835	0.0091	0.0035	0.0455	0.0039	32	19	68	412	622	21	404.7516705	7.24833
19	0.917	0.0073	0.0028	0.0427	0.0031	31	22	71	408	673	25	415.9733639	-7.973364
20	0.9471	0.0074	0.0029	0.0138	0.0032	31	22	72	418	653	18	419.1758176	-1.175818
21	0.9391	0.0071	0.0028	0.0143	0.0031	32	21	75	437	697	17	415.5577758	21.44222
Fig	ure (16-a) Tes	sting	the p	oredi	ictio	n mo	del a	nd ca	lculat	ing the 1	nean
-			e	rror	in nre	dict	tion (of vi	eld st	ress		-	
00		0.00700			a ana			JI yr	ciu st			446 7040000	00 700

22	0.91695	0.00729	0.00281	0.01563	0.00313	31	21	70	394	639	20	416,7019989	-22.702
23	0.60376	0.01208	0.00466	0.05175	0.00518	29	21	86	433	655	26	423.6505009	9.349499
24	0.98945	0.00761	0.00294	0.02936	0.00326	31	20	77	374	564	21	408.822292	-34.82229
25	0.98957	0.00753	0.0029	0.03012	0.00323	35	25	75	410	658	20	421.4346299	-11.43463
26	0.65127	0.01018	0.00275	0.05495	0.00305	34	14	72	387	595	22	383.049877	3.950123
27	0.96618	0.02196	0.01186	0.24155	0.01318	37	18	66	379	593	21	386.6047265	-7.604727
28	0.9711	0.00819	0.00316	0.0585	0.00351	30	19	69	370	554	26	401.831541	-31.83154
29	0.93779	0.00729	0.00281	0.04168	0.00313	35	21	74	388	609	20	408.4935568	-20.49356
30	0.93594	0.0113	0.00436	0.04841	0.00484	35	25	73	380	626	20	418,4670446	-38,46704
31	0.98802	0.00865	0.00333	0.0457	0.00371	25	11	66	365	546	24	380.8169657	-15.81697
32	0.98989	0.00729	0.00281	0.0521	0.00313	32	20	74	403	651	19	404.3840122	-1.384012
33	0.95683	0.00761	0.00294	0.05437	0.00326	29	18	81	399	597	18	401.8155363	-2.815536
34	0.98934	0.00769	0.00297	0.05496	0.0033	35	14	75	409	676	16	381.1411868	27.85881
35	0.78927	0.01036	0.00266	0.04933	0.00296	34	19	77	376	608	21	394.0055618	-18.00556
36	0.73921	0.00761	0.00315	0.04348	0.00326	31	15	98	358	559	22	403.1300403	-45.13004
37	0.98958	0.00729	0.00313	0.04167	0.00313	43	15	73	401	633	21	381.7134167	19.28658
38	0.70409	0.00761	0.00285	0.04757	0.00285	26	23	62	444	627	16	429.7644283	14.23557
39	0.9861	0.0105	0.0034	0.0479	0.0029	26	18	68	343	537	23	395.1874333	-52.18743
40	0.9717	0.0223	0.0061	0.081	0.0061	25	18	75	393	573	24	369.5373217	23.46268
41	0.3457	0.0296	0.0074	0.0741	0.0074	28	17	78	371	556	22	371.2762463	-0.276246
42	0.9864	0.0099	0.0037	0.0493	0.0037	24	12	98	406	660	19	385.0525795	20.94742

Figure (16-b) Testing the prediction model and calculating the mean error in prediction of yield stress

43	0 70303	0.01105	0.00400	0.07032	0.00422	33	18	1.01	407	681	26	396,4258267	10.57417
	0.98806		0.00326	0.04886		35		87	400	626	20	388.0543451	11.94565
44							16						
45				0.04791		38	2	84	426	664	18	337.1156404	88.88436
46			0.00376	0.05373		31	24	72	350	542	23	425.3389162	-75.33892
47	0.98684	0.00987	0.00329	0.05482	0.00329	36	19	84	326	499	25	391.5410206	-65.54102
48	0.97959	0.01633	0.00408	0.06803	0.00408	33	17	109	366	565	22	368.9633033	-2.963303
49	0.95238	0.03741	0.0102	0.10204	0.0102	33	21	76	364	584	22	345.6402538	18.35975
50	0.96691	0.00859	0.00301	0.05372	0.00322	24	26	74	348	537	22	428.8496288	-80.84963
51	0.98253	0.01365	0.00382	0.05459	0.00328	37	21	87	385	608	23	387.0096552	-2.009655
52	0.97986	0.01633	0.00381	0.05444	0.00327	33	18	91	397	598	20	370.3858817	26.61412
53	0.98793	0.00878	0.00329	0.05488	0.00329	29	13	90	411	626	23	382.9575822	28.04242
54	0.98446	0.01244	0.00311	0.05181	0.00311	32	24	79	405	636	19	400.1594826	4.840517
55	0.98446	0.01244	0.00311	0.05181	0.00311	38	22	78	392	630	20	387.8626238	4.137376
56	0.98691	0.01007	0.00302	0.05035	0.00302	40	18	80	384	619	20	381.6989916	2.301008
57	0.9838	0.01273	0.00347	0.05787	0.00347	38	17	89	413	679	25	373.2277572	39.77224
58	0.98542	0.01106	0.00352	0.06033	0.00302	29	14	88	397	633	20	378.0658215	18.93418
59	0.98571	0.01084	0.00345	0.04929	0.00296	36	20	82	376	591	27	392.905752	-16.90575
60	0.982	0.0149	0.0031	0.0534	0.0032	33	12	89	355	632	25	349.9460077	5.053992
61	0.9821	0.0149	0.003	0.0595	0.003	28	17	97	329	500	25	369.9512044	-40.9512
62	0.8673	0.0071	0.0031	0.0561	0.0031	35	20	101	424	637	20	410,3080786	13.69192
63	0.7668	0.0124	0.0031	0.0518	0.0031	38	21	81	429	629	19	393.1831321	35.81687

Figure (16-c) Testing the prediction model and calculating the mean error in prediction of yield stress.

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	0.9768	0.01954	0.00366	0.06105	0.00366	33	18	91	390	<u>631</u>	20	rolling t	34.3929
64 65	0.97622	0.02003	0.00366 0.00375 0.00343	0.06258	0.00375	33	18	81	409	645	24	353.5394251	55.4605
66 67	0.98874	0.01365	0.00328	0.04895	0.00294	35 28	29 21	83 80	417 381	652 566	18 22	435.4950821 390.2704622	-18.4950 -9.27046
68 69	0.9781	0.01752	0.00247	0.05839	0.00438	32	11 21	110 97	380 407	578 610	22 20	349.4860475 405.9802648	30.5139 1.01973
70 71	0.76844	0.01332		0.05123	0.00307	35	18	92 89	422 413	650 627	19 19	383.0096408 393.6385286	38.9903 19.3614
72 73	0.72131	0.01311	0.00328	0.05464	0.00328	31	20	89 96	399 429	594 680	21 19	397.0946412 382.1076836	1.90535
74 75	0.63102	0.01283	0.00321	0.05348	0.00321	24 33	19	72 96	415 411	628 629	20	403.2727285 374.982981	11.7272
76	0.98305	0.01356	0.00339	0.0678	0.00339	34	22	110	438	730	17	389.5041895	48.4958
77 78	0.65502	0.01419	0.00328	0.06004	0.00347	31	14	86	415 359	545	19 22	382.9536005 372.9855531	32.0464 -13.9855
79 80	0.72821	0.01231	0.00308	0.05128	0.00308	30	111	100	429 413	663 655	20 19	701.9348595 402.0424093	-272.934
81 82	0.9891	0.0079	0.003	0.0495	0.003	33 29	17	92 79	413 401	633 643	20	393.9828195	19.0171
83	0.9896	0.0073	0.0031	0.0417	0.0031	38	19	85	407	635	19 19	405.2184647 400.4877448	-4.21846 6.51225
84 Tigu	0.7448 ure (0.011 16-d		0.0438 sting		32 ored	12 ictio	66 n mo	433 odel a	668 nd ca	lcula	ting the	55.5337 mean
			e	rror	in pre	edic	tion	of yi	eld st	ress.			
85 86	0.98649	0.00869	0.00266	0.04343	0	33 30	25 20	79 83	386 412	566 611	22 19	428.8069773 390.5942768	-42.8069 21.4057
87 88	0.86482	0.00769	0.00297	0.22758	0.01365	27 31	21 22	87 81	364 383	557 657	23 20	377.6481785 411.8034002	-13.6481 -28.8034
89 90	0.98968	0.00745		0.05321	0.00319	28 34	24 21	84 81	494 380	535 603	20 20	421.8345612 390.6591127	72.1654
91	0.98979	0.00737	0.00284	0.04212	0.00316	35	18	76	425	738	18	396.5776793	28.4223
93	0.93458	0.0113	0.00328	0.05135	0.00308	36	18	78	384	601	20	380.1894576	3.81054
94 95	0.98501		0.00321	0.05298	0.00318	30 33	25 15	81 83	386 376	586 599	20 21	406.3233932 372.9634722	-20.3233 3.03652
96 97	0.70855	0.00729	0.00292		0.00313 0.00313	32 32	23 19	81 76	400 369	702 623	19 21	425.7053696 402.0977621	-25.7053 -33.0977
98 99	0.9009	0.07207	0.00317	0.05291	0.02703 0.00317	36 36	22 17	82 85	400 374	602 578	19 26	340.3200114 373.0436125	59.6799 0.95638
100	0.98462		0.00308	0.05231	0.00308	34 31	20	77	418 431	645 673	19 21	385.0462783 406.1587524	32.9537
102	0.6483	0.0093	0.0028	0.0525	0.0031	34	25	80	372	580	21	424.4793327	-52.4793
103 104 105	0.973	0.0189 0.017 0.008	0.0081 0.0043 0.0027	0.0811 0.0709 0.05	0.0081 0.0043 0.003	31 22 29	17 17 22	70 64 92	425 390 419	650 542 654	17 26 19	391.6320445 374.3698511 422.4369891	33.3679 15.6301 -3.43698
) Tes	sting	the p	ored	ictio	n mo	del a	nd ca		ting the	
A.J 106	DRI 0.96901	FeMn 0.00808	FeSi	Lime 0.04038	Dol.	C 31	Si 20	01 y1	eld st بيد الغضرع 430	ress. قرة الشد ، 678	الاستطالة% 20	د الخضوع المتوقع 404.2098025	فاء التوقع جو 25.7902
107	0.94145	0.00686	0.00265	0.04903	0.00294	31 33	21 21	77 84	414 391	641 677	19 20	411.4253639 409.638562	2.57463
109	0.98989	0.00729	0.00281	0.0521	0.00313	41	20	90 70	395 410	644 698	20 19	397.1264814 407.1546003	-2.12648
111	0.93642	0.01387	0.00347	0.0578	0.00347	30	20	84	385	605	23	387.5167457	-2.51674
112	0.94767	0.00737	0.00284	0.04738	0.00316	39 36	32 20	90 83	401 427	661 690	19 20	441.049331 404.0844603	-40.0493 22.9155
114	0.97337	0.00946	0.00365	0.05543 0.04151	0.00406	31 33	22 23	76	399 382	612 606	20 20	410.9968815 418.6575007	-11.9968
116	0.98662	0.01075	0.00264	0.03907	0.00293	33 32	24	78 84	380	539 530	26 25	403.7156577 381.8414871	-23.7156
118	0.70104	0.01753	0.00394	0.07302	0.00438	31	23	82	387	596	20	392.9599768	-5.95997
119 120	0.98548	0.01096	0.00296	0.05478	0.00329	29 32	22 17	88 70	439 314	678 636	18 22	401.1882326 377.1707662	37.8117 -63.1707
121 122	0.98593	0.0113	0.00277	0.05135	0.00308	32	21	83	421 409	653 636	18 21	392.2312411 389.4649686	28.7687
123	0.9805	0.0159	0.0036	0.0663	0.004	24	24	81 75	398 466	658 776	21 15	396.1949367 375.7947745	1.80506
125	0.9829	0.0142	0.0029	0.0546	0.0033	30 37	19 20	80 75	396 438	622 683	21 18	376.8487669 377.1855728	19.1512
igu											lcula	ting the	mean
127	0.98437	0.0123	0.00332	0.03691	0.00369	26 34	25	75 100	eld st	629 633	18 23	413.6260311 422.6683865	14.3739
129 130	0.98578	0.01141	0.0028		0.00311	30 34	22 24	78	376 380	582 638	24	396.7655073 407.8153524	-20.7655
131	0.98619	0.01127	0.00254	0.04696	0.00282	31	18	76	339	548 672	24	381.3765863	-42.3765
133	0.98708	0.01018	0.00275	0.05088	0.00305	30	19	79	419	637	20	391.4729126	27.5270
134 135	0.99456	0.00262	0.00313	0.04188	0.00314	33 37	20 26	73	431 465	695 734	18 16	389.8899233 440.2195313	41.1100 24.7804
136 137	0.98361	0.01311	0.00328	0.05464	0.00328	31 31	23	69 77	441 386	671 619	20 24	395.456127 402.2681148	45.5438
138	0.98731	0.00976	0.00293		0.00325	34	23	74	353 416	5599 703	25	405.0254027 389.692158	-52.025
140		0.01274	0.00313	0.04631	0.00347	31	15	79	401	680	19	371.2290294	29.7709
141 142	0.98746		0.00321			28 30	21 19	74	397 419	684 636	20 21	402.1895421 392.7882232	-5.18954 26.2117
143		0.01247	0.00374		0.00416	28	21	86	408	634 635	19 19	399.5769747 407.2388668	8.42302
145	0.9899	0.0073	0.0028	0.0417		31	20	74	355	561	22	406.8991756	-51.8991
146 147	0.6752	0.0104	0.0028 0.0028	0.0623	0.0031	30 33 redi	21 19	82 73	435 381 del ai	688 663 nd ca	20 20 1cula	411.2421037 398.2354075 ting the	23.757 -17.2354 mean
0			e	rror	in pre				eld st			C	
148 149 150	0.98614	0.01		0.05717	0.00429 0.00357	31 29 36	21 21 20	88 81 114	392 403 386	635 617 595	20 19 25	404.0321499 408.8455243 401.8464497	-12.0321 -5.84552 -15.8464
151 152		0.00987		0.0395	0.00296	31 32	21 27	82 72	393 390	529 607	20 27	383.9119763 417.7995811	9.08802
153 154	0.9901	0.00715			0.00306	34	24	74	405	624 614	24 20	416.0045408 409.9512312	-11.0045
155	0.70479	0.00796		0.01819	0.00341	33 34	23	82	431 437	670	18	429.7632555 404.1407597	1.23674
157	0.5735	0.01096	0.00228	0.05482	0.00253	30	22	76	374	602	21	409.2536774	-35.2536
158 159			0.00281	0.04159	0.00328	31 29	19 22	77 81	381 432	603 642	20 18	383.2928018 408.8794981	-2.29280 23.1205
160 161		0.00834	0.00322		0.00326	34 32	23 19	86	461 409	743 643	17 20	423.9503798 421.3782548	37.0496 -12.3782
162	0.98517	0.01191	0.00292	0.06496		30 29	22 18	92 87	362 394	581 627	22 23	394.9087739 413.5961202	-32.9087 -19.5961
164	0.60024	0.00934		0.04402	0.004	24 30	17 22	76	400	615 686	19	417.206216 419.9150193	-17.2062
166	0.9691	0.0073	0.0028	0.0417	0.0031	37	23	75	438	667	19	412.1138629	25.8861
167 168	0.9368	0.0076	0.0632		0.0703	32 32	25 15	79 80	468 479	755 717	16 15	423.2897784 930.2204766	44.7102 -451.220
ıgı	ure (16-g							odel a eld st		icula	ting the	mean
169 170	0.98787	0.00875	0.00338			29 34	20 23	77	456 417	778	17 19	405.0720882 414.8314527	50.9279 2.16854
171	0.9891	0.00787	0.00303	0.03934	0.00337	27	19	72	410	663	19	407.2401	2.7599
172 173	0.73551	0.00686	0.00297	0.03923	0.0033	26 28	22 23	75	455 513	707 778	17 16	417.7104545 429.9490812	37.2895 83.0509
174			0.00307		0.00341	33 30	24	77	462 459	666	16 17	418.0228131 409.7292477	43.9771 49.2707
176	0.98979	0.00722	0.00278	0.05155	0.00309	32	23	73	433	656	20	414.3803016	18.6197
177	0.986		0.004		0.00349	28 30	17 17	68 74	420 448	691 697	20 17	396.8120375 397.7125745	23.1879 50.2874
	0.97914	0.0149	0.00596	0.08514	0.00639	28	19	92	364	553 634	22	398.9990387	-34.9990
179 180	0.98383	0.01167	0.0045	0.0667	0.005	34	20	82	419		19	398.639748	20.3602
	0.98934	0.00769	0.0045	0.05496	0.0033	34 32 23	20 20 18	82 73 64	419 397 479	681 762	19 22 17	398.639/48 403.6734546 390.8797683	-6.67345
180 181 182 183	0.98934 0.99069 0.6462	0.00769 0.00788 0.01346	0.00297 0.00143 0.00377	0.05496 0.05629 0.05385	0.0033 0.00338 0.00404	32 23 34	20 18 15	73 64 103	397 479 374	681 762 639	22 17 22	403.6734546 390.8797683 384.8339449	20.3602 -6.67345 88.1202 -10.8339
180 181 182	0.98934 0.99069 0.6462 0.97349 0.98698	0.00769 0.00788 0.01346 0.02071 0.01018	0.00297	0.05496 0.05629 0.05385 0.06214 0.0407	0.0033 0.00338 0.00404 0.00621 0.00305	32 23	20 18	73 64	397 479	681 762	22 17	403.6734546 390.8797683	-6.67348 88.1202

						Δ.	orano	Predict	ion Erroi	= 2 929	656		
197	0	0.03186	0.01229	0.22758	0.01365	30	16	76	433	787	18	390.9556703	42.04433
196	0	0.02595	0.01001	0.18539	0.01112	31	27	88	378	610	21	437.0503779	-59.0503
195	0.7475	0.00769	0.00297	0.04397	0.0033	30	17	82	448	744	17	407.2701825	40.72982
194	0.98796	0.00926	0.00278	0.04116	0.00309	30	22	72	437	703	18	406.2842606	30.71574
193	0.98968	0.00745	0.00287	0.04257	0.00319	30	24	81	444	606	17	421.3688381	22.63116
192	0.98979	0.00737	0.00284	0.04212	0.00316	33	20	77	433	726	18	405.1409158	27.85908
191	0.77837	0.00841	0.00284	0.04207	0.00316	30	17	73	402	605	19	401.6996346	0.30036
190	0.93306	0.00976	0.00293	0.0434	0.00325	39	21	87	423	672	19	396.7607883	26.2392

Figure (16-i) Testing the prediction model and calculating the mean error in prediction of yield stress.

From Figure (16) the prediction process for yield stress was carried out for 197 samples and the average error was very small 2.928656 compared to the sample size 197 and the mean error sign was positive and this indicates that the real value is greater than the prediction value, so we increased the mean error to the prediction to get On average error equal to zero.

3.3 Testing the Tensile Strength Prediction Model:

Test the prediction model and calculate the average error in predicting the tensile strength, and these results are shown in Figure (17) for all 198 samples obtained from the prediction model.

NO	DRI	FeMn	FeSi	Lime	Dol.	С	Si	Mn	Yield	Tensile	Fist of	Expected Yi	eld Error
1	0.93647	0.00745	0.00287	0.04363	0.00319	34	23	81	Effort	Strengt	Elongatio	n Effort	80117
2	0.93779	0.00729	0.00281	0.04897	0.00313	31	19	75	429	668	17	634.0081868	33.99181
3	0.66688	0.00729	0.00281	0.04168	0.00313	30	20	74	431	681	18	619.9045078	61.09549
4	0.93579	0.00753	0.0029	0.0484	0.00323	32	21	70	450	673	21	640.8586352	32.14136
5	0.95863	0.00729	0.00281	0.0521	0.00313	30	22	72	475	771	15	650.5047386	120.4953
6	0.9244	0.00886	0.00342	0.05065	0.0038	30	19	80	384	619	20	645.6264589	-26.62646
7	0.93579	0.00753	0.0029	0.04302	0.00323	31	18	77	412	653	19	631.4085979	21.5914
8	0.59473	0.04248	0.02294	0.08496	0	29	22	76	457	700	16	686.913766	13.08623
9	0.84966	0.00959	0.0037	0.05482	0	32	21	75	382	583	26	656.3976541	-73.39765
10	0.9289	0.00834	0.00322	0.05955	0.00357	29	23	79	452	732	16	677.5308601	54.46914
11	0.75023	0.007	0.0027	0.05002	0.003	33	24	70	428	692	17	663.3158914	28.68411
12	0.8651	0.00631	0.00243	0.03514	0.0027	30	26	74	442	717	20	693.9831872	23.01681
13	0.94875	0.00722	0.00278	0.04125	0.00309	32	25	76	419	650	19	703.6638175	-53.66382
14	0.94087	0.00693	0.00267	0.04457	0.00297	35	18	74	442	712	22	638.1818323	73.81817
15	0.69409	0.00715	0.00276	0.0347	0.00306	33	26	70	444	729	17	681.6208495	47.37915
16	0.9329	0.00787	0.00303	0.0562	0.00337	34	23	72	394	651	20	675.1227637	-24.12276
17	0.8904	0.00769	0.00297	0.05496	0.0033	34	21	74	370	613	21	659.4309267	-46.43093
18	0.8835	0.0091	0.0035	0.0455	0.0039	32	19	68	412	622	21	610.3628864	11.63711
19	0.917	0.0073	0.0028	0.0427	0.0031	31	22	71	408	673	25	649.7066605	23.29334
20	0.9471	0.0074	0.0029	0.0138	0.0032	31	22	72	418	653	18	658.5194648	-5.519465
21	0.9391	0.0071	0.0028	0.0143	0.0031	32	21	75	437	697	17	662.6081195	34.39188

0			·	0								U	
			e	rror	in pro	edic	ting	the t	ensile	strei	ngth.		
22	0.91695	0.00729	0.00281	0.01563	0.00313	31	21	70	394	639	20	639.4265376	-0.42653
23	0.60376	0.01208	0.00466	0.05175	0.00518	29	21	86	433	655	26	660.7476296	-5.74763
24	0.98945	0.00761	0.00294	0.02936	0.00326	31	20	77	374	564	21	656.5640492	-92.5640
25	0.98957	0.00753	0.0029	0.03012	0.00323	35	25	75	410	658	20	716.7018275	-58.7018
26	0.65127	0.01018	0.00275	0.05495	0.00305	34	14	72	387	595	22	560.2204891	34.77951
27	0.96618	0.02196	0.01186	0.24155	0.01318	37	18	66	379	593	21	609.4748475	-16.4748
28	0.9711	0.00819	0.00316	0.0585	0.00351	30	19	69	370	554	26	609.7101182	-55.7101
29	0.93779	0.00729	0.00281	0.04168	0.00313	35	21	74	388	609	20	668.3872533	-59.3872
30	0.93594	0.0113	0.00436	0.04841	0.00484	35	25	73	380	626	20	703.0552519	-77.0552
31	0.98802	0.00865	0.00333	0.0457	0.00371	25	11	66	365	546	24	500.2729844	45.72702
32	0.98989	0.00729	0.00281	0.0521	0.00313	32	20	74	403	651	19	647.7709228	3.229077
33	0.95683	0.00761	0.00294	0.05437	0.00326	29	18	81	399	597	18	636.8178465	-39.8178
34	0.98934	0.00769	0.00297	0.05496	0.0033	35	14	75	409	676	16	603.0751032	72.9249
35	0.78927	0.01036	0.00266	0.04933	0.00296	34	19	77	376	608	21	636.5196068	-28.5196
36	0.73921	0.00761	0.00315	0.04348	0.00326	31	15	98	358	559	22	662.8197844	-103.819
37	0.98958			0.04167		43	15	73	401	633	21	643.6364033	-10.6364
38	0.70409	0.00761	0.00285	0.04757	0.00285	26	23	62	444	627	16	593.1373675	33.86263
39	0.9861	0.0105	0.0034	0.0479	0.0029	26	18	68	343	537	23	578.3803834	-41.3803
40	0.9717	0.0223	0.0061	0.081	0.0061	25	18	75	393	573	24	580.9595089	-7.95950
41	0.3457	0.0296	0.0074	0.0741	0.0074	28	17	78	371	556	22	545.2677191	10.73228
42	0.9864	0.0099	0.0037	0.0493	0.0037	24	12	98	406	660	19	616.2162295	43.78377
												616.2162295	

Figure (17-b) Testing the prediction model and calculating the mean

41	0.3457	0.0296	0.0074	0.0741	0.0074	28	17	78	371	556	22	545.2677191	10.73228
40		0.0223				25	18	75	393	573	24	580.9595089	-7.959509
39	0.9861	0.0105	0.0034	0.0479	0.0029	26	18	68	343	537	23	578.3803834	-41.38038
38				0.04757		26	23	62	444	627	16	593.1373675	33.86263
37	0.98958	0.00729	0.00313	0.04167	0.00313	43	15	73	401	633	21	643.6364033	-10.6364
36	0.73921	0.00761	0.00315	0.04348	0.00326	31	15	98	358	559	22	662.8197844	-103.8198
35	0.78927	0.01036	0.00266	0.04933	0.00296	34	19	77	376	608	21	636.5196068	-28.51961
34	0.98934	0.00769	0.00297	0.05496	0.0033	35	14	75	409	676	16	603.0751032	72.9249
33				0.05437		29	18	81	399	597	18	636,8178465	-39.81785
32				0.0521		32	20	74	403	651	19	647.7709228	3.229077
30		0.00865			0.00484	25	11	66	365	546	20	500.2729844	45.72702
29		0.00729		0.04168		35	21 25	74	388 380	609 626	20 20	668.3872533 703.0552519	-59.38725 -77.05525
28	0.9711			0.0585		30 35	19	69 74	370	554	26	609.7101182 668.3872533	-55.71012
27				0.24155		37	18	66	379	593	21	609.4748475	-16.47485
26				0.05495		34	14	72	387	595	22	560.2204891	34.77951
25				0.03012		35	25	75	410	658	20	716.7018275	-58.70183
24	0.98945	0.00761	0.00294	0.02936	0.00326	31	20	77	374	564	21	656.5640492	-92.56405
23	0.60376	0.01208	0.00466	0.05175	0.00518	29	21	86	433	655	26	660.7476296	-5.74763
22	0.91695	0.00729		0.01563		31	21	70	ensile	639	20	639.4265376	-0.426538

Figure (17-c) Testing the prediction model and calculating the mean error in predicting the tensile strength.

36.00566 35.01328

0 0635

0.4354 0.0096 0.0029 0.0637 0.0032

0.7958 0.0101 0.0027 0.0403 0.003

189 0 667 0.0111

82 76 83

706 747 727

435 443

18 18 17

Use of Multiple Linear Regression Technology in Controlling the Technical Specifications of Industrial Products...

324.0314 -39.15748 Azouza & Naser

	0.68985	0.01054	0.00326	0.04886	0.00326	30	10	8/	400	664	20	499.7830106	-33.10/48
45	0.98872	0.00752	0.00259	0.05373	0.00287	38	2	84 72	426	542	18 23	681.959527	164.217
47	0.98684	0.00987	0.00329	0.05482	0.00329	36	19	84	326	499	25	685.885907	-186.8859
48	0.97959	0.01633	0.00408	0.06803	0.00408	33	17	109	366	565	22	727.5867451	-162.5867
49	0.95238	0.03741	0.0102	0.10204	0.0102	33	21	76	364	584	22	632.233921	-48.23392
50	0.96691	0.00859	0.00301	0.05372	0.00322	24	26	74	348	537	22	670.9336215	-133.9336
51	0.98253	0.01365	0.00382	0.05459	0.00328	37	21	87 91	385 397	608 598	23	715.4105513 676.1111788	-107.4106 -78.11118
53		0.00878	0.00329	0.05488	0.00327	29	13	90	411	626	23	619.3450093	6.654991
54	0.98446	0.01244	0.00311	0.05181	0.00311	32	24	79	405	636	19	695.5444127	-59.54441
55	0.98446	0.01244	0.00311	0.05181	0.00311	38	22	78	392	630	20	697.2696582	-67.26966
56	0.98691	0.01007	0.00302	0.05035	0.00302	40	18	80	384	619	20	677.540762	-58.54076
57	0.9838	0.01273	0.00347	0.05787	0.00347	38	17	89	413	679	25	685.6021559	-6.602156
58	0.98542	0.01106	0.00352	0.06033	0.00302	29	14	88	397	633	20	618.3856016	14.6144
60	0.98571	0.01084	0.00345	0.04929	0.00296	36	20	82	376	591 632	27	688.8664896	-97.86649
						33			355		25	607.7155203	24.28448
61	0.9821	0.0149	0.003	0.0595	0.003	28	17	97	329	500	25	663.5853314	-163.5853
62	0.8673	0.0071	0.0031	0.0561	0.0031	35	20	101	424	637	20	747.752439	-110.7524
63	0.7668	0.0124	0.0031	0.0518	0.0031	38	21	81	429	629	19	683.6916234	-54.69162
Fig	ure (17-d) Te	sting	the 1	ored	ictio	n mo	odel ar	nd ca	lcula	ting the	mean
0	```			-								0	
			e	rror	in pr		ung	the t	ensile		ngtn.		
64	0.9768	0.01954	0.00366	0.06105	0.00366	33	18	91	390	631	20	666.6067465	-35.60675
65		0.02003		0.06258		33	18	81	409	645	24	631.0830913	13.91691
66	0.98874	0.00783		0.04895	0.00294	35	29	83	417	652	18	785.3719884	-133.372
67	0.98307		0.00328			28	21	80	381	566	22	649.7266736	-83.72667
68	0.9781		0.00438			32	11	110	380	578	22	666.4652895	-88.46529
69	0.78254			0.04119	0.00247	35	21	97	407	610	20	733.0207413	-123.0207
70				0.05123	0.00307	35	18	92	422	650	19	677.0771933	-27.07719
71			0.00298			34	21	89	413	627	19	694.9203126	-67.92031
72	0.9865	0.01311	0.00328	0.05464	0.00328	31 33	20	89 96	399 429	594 680	21 19	667.9865038 682.9959919	-73.9865 -2.995992
74			0.00312			24	19	72	425	628	20	564.0583962	63.9416
75			0.00296			33	13	96	411	629	20	633.3030874	-4.303087
76			0.00339	0.0678	0.00339	34	22	110	438	730	17	788.3660632	-58,36606
77	0.73988	0.01387	0.00347	0.0578	0.00347	33	17	92	415	696	19	656.7722693	39.22773
78			0.00328		0	31	14	86	359	545	22	594.0033288	-49.00333
79	0.72821	0.01231	0.00308	0.05128	0.00308	30	111	100	429	663	20	1618.410021	-955.41
80			0.00305			36	19	94	413	655	19	689.5312985	-34.5313
81	0.9891	0.0079	0.003	0.0495	0.003	33	17	92	413	633	20	684.3442287	-51.34423
82	0.9894		0.003	0.0414	0	29	19	79	401	643	19	648,2708671	-5.270867
83	0.9896	0.0073	0.0031	0.0417	0.0031	38	19	85	407	635	19	704 3964006	-69 3964
84	0.7448	0.011		0.0417		32	12	66	433	668	19	519 6021884	148.3978
Fig	ure (17-е) Tes	sting	the t	predi	ictio	n mo	odel ar	ıd ca	dcula	ting the	mean
	(-								0	
			e	rror	in pro	edici	ting i	the t	ensile	stre	ngth.		
85	0.76004	0.00869	0.00326			33	25	79	386	566	22	705.5055693	-139,5056
86			0.00266		0	30	20	83	412	611	19	665.7058631	-54.70586
87	0.86482	0.03186	0.01229	0.22758	0.01365	27	21	87	364	557	23	645.7486052	-88.74861
88	0.98934	0.00769		0.05496	0.0033	31	22	81	383	657	20	687.451713	-30.45171
89	0.98968	0.00745		0.05321	0.00319	28	24	84	494	535	20	705.6183067	-170.6183
90			0.00289			34	21	81	380	603	20	681.8237663	-78.82377
91			0.00284			35	18	76	425	738	18	648.4185386	89.58146
92	0.98468		0.00328			33	20	92	413	657	21	707.3982976	-50.3983
93	0.93458			0.05135		36	18	78	384	601	20	645.8996634	-44.89966
94			0.00286			30	25	81	386	586	20	704.0898705	-118.0899
95	0.98501		0.00321	0.05353	0.00321	33	15	83	376	599	21	624.9688477	-25.96885
96 97	0.98979		0.00281			32	23		400 369	702 623	19	684.2048313	17.79517
97			0.00292			32	19	76	400	623	21 19	645.3122808 667.2665748	-22.31228 -65.26657
99	0.98413			0.05291		36	17	85	374	578	26	662.454297	-84.4543
100	0.98462	0.01231	0.00308	0.05231	0.00308	34	20	77	418	645	19	656.895051	-11.89505
100	0.9867		0.00333			31	20	87	431	673	21	705.2324479	-32.23245
102			0.0028			34	25	80	372	580	21	700.8493419	-120.8493
102	0.973		0.0020			31	17	70	425	650	17		53,23034
103	0.973					22			420			596.7696631	
		0.017		0.0709			17	64		542	26	524.0385065	17.96149
105	0.7095		0.0027	0.05	0.003	29	22	92	419	654	19	697.8530348	-43.85303
Figu	ure (17-t) Tes	ting	the p	predi	ct101	n mo	del ar	id ca	lcula	ting the	mean
				-	. ~							0	
					in pro	eaici	ting i	the t	ensile	stre			
106	0.96901		0.00273	0.04038	0.00303	31	20	77	430	678	20	651.8609478	26.13905
107	0.94145		0.00265	0.04903	0.00294	31	21	77	414	641	19	661.4046543	-20.40465
108	0.9901	0.007	0.0029	0.05001	0.003	33	21	84	391 395	677 644	20 20	698.3534326 741.2303876	-21.35343 -97.23039
109	0.98989	0.00729	0.00281		0.00313	41 32	20	90	395	644 698	20	741.2303876 641.5578491	-97.23039 56.44215
111	0.93642	0.01387	0.00312	0.05203	0.00347	30	20	84	385	605	23	659.1110374	-54.11104
112	0.94767	0.00737	0.00284		0.00316	39	32	90	401	661	19	851.2796901	-190.2797
113	0.95863	0.00729	0.00281	0.04168	0.00313	36	20	83	427	690	20	695.107292	-5.107292
114	0.97337	0.00946	0.00365	0.05543	0.00406	31	22	76	399	612	20	668.5182954	-56.5183
115	0.70179	0.0089	0.00267	0.04151	0.00297	33	23	77	382	606	20	671.1140475 698.9167479	-65.11405
116	0.98662		0.00264	0.03907	0.00293	33	24	78	380	539 530	26 25	698.9167479 653.7813308	-159.9167 -123.7813
117	0.98427		0.00289			32	18	84	385	530 596	25 20	653.7813308 663.4736931	-123.7813 -67.47369
119	0.98609	0.01096	0.00296	0.05478	0.00329	29	22	88	439	678	18	695,8518629	-17.85186
120	0.98548	0.01166	0.00286	0.05298	0.00318	32	17	70	314	636	22	593.9334596	42.06654
121	0.98593	0.0113	0.00277	0.05135	0.00308	32	21	83	421	653	18	679.8261964	-26.8262
122			0.00269			31	16	90	409	636	21	634.7778433	1.222157
123			0.0036			24	24	81	398	658	21	661.0143757	-3.014376
124			0.0026			36	18	75	466	776	15	637.6531836	138.3468
125			0.0029			30	19	80	396	622	21	634.7530571	-12.75306
126	0.9838	0.0133	0.003	0.0553	0.0033	37	20	75	438	683	18	659.1995898	23.80041
Fig	ure (17-ø) Te	sting	the 1	ored	ictio	n me	odel ar	nd ca	lcula	ting the	mean
8'		- 8			-							8 410	
			e	rror	in pr	edict	ting	the t	ensile	stre	ngth.		
127	0 98437	0.0192	0.00332	0.03694	0.00369	26	25	75	428	629	18	669.1252991	-40.1253
127					0.00369	34	20	100	374	633	23	743,819434	-40.1255
129	0.98578	0.01141	0.0028	0.05188	0.00311	30			376	582	24	663.9111568	-81.91116
130	0.7124	0.01171	0.00263	0.04879	0.00293	34	24	75	380	638	20	671.8590522	-33.85905
131	0.98619	0.01127	0.00254	0.04696	0.00282	31	18	76	339	548	24	620.5822683	-72.58227
132	0.97168	0.02082	0.0075	0.05552	0.00833	33		76	416	672	19	660.8357446	11.16426
133	0.98708	0.01018	0.00275	0.05088	0.00305	30		79	419	637	20	639.8910875	-2.891088
134	0.98414	0.01274	0.00313	0.01737	0.00347	33	20	73	431	695	18	641.8294755	53.17052
135	0.99456	0.00262	0.00283	0.04188	0.00314	37		80 69	465	734	16	761.9262527	-27.92625
136						31			441	671	20	645.5562409	25.44376
137 138	0.98754	0.00959	0.00288	0.03835	0.00288	31 34	21 23	77	386 353	619 5599	24 25	661.1439564 682.3552367	-42.14396 4916,645
138	0.98731	0.009/6	0.00293	0.0434	0.00325	34 29	19	94	353 416	703	25 19	682.3552367	4916.645
	0.98414					31	15	79	401	680	19	600.4776516	79.52235
140	0.9861	0.01069	0.00321	0.04752	0.00356	28	21	74	397	684	20	635.7109627	48.28904
142	0.98746	0.00987	0.00267	0.04246	0.00356	30	19	73	419	636	21	620.3691551	15.63084
143	0.98379	0.01247	0.00374	0.05542	0.00416	28	21	86	408	634	19	674.9749085	-40.97491
144	0.9904	0.0069	0.0027	0.0416	0.003	31	20	76	409	635	19	651.8855838	-16.88558
145	0.9899	0.0073	0.0028	0.0417	0.0031	31	20	74	355	561	22	644.8011639	-83.80116
146	0.9899	0.0073	0.0028	0.0448	0.0024	20	21	82	435	688	20	678.0171197	9.98288
				0.0000	0.0004		19	73	381	663	20	610.206722	52.79328
147	0.6752	0.0104	0.0028	0.0623	0.0031	- 33	19						52.79328
		· · · · ·										ting the	

0.70323 0.01125 0.00422 0.07032 0.00422 0.98806 0.00869 0.00326 0.04886 0.00326 0.06885 0.0154 0.00326 0.04886 0.00326

43 44 45

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18 1.01 16 87

Figure (17-i) Testing the prediction model and calculating the mean error in predicting the tensile strength.

148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166	0.97787 0.98746 0.9891 0.70479 0.75556 0.5735 0.98501 0.95664 0.76112 0.30963 0.98517 0.66688 0.60024	0.01251 0.01 0.00834 0.00987 0.00987 0.00785 0.00745 0.01096 0.01204 0.00936 0.00761 0.00834 0.00834 0.01191	0.00386 0.00322 0.00463 0.00267 0.00276 0.00303 0.00307 0.00287 0.00228 0.00296 0.00281 0.00294 0.00224	0.06862 0.0395 0.05104 0.0562 0.01819 0.01703 0.05482 0.06129 0.04159	0.00515 0.00296 0.00306 0.00337 0.00341 0.00319 0.00253 0.00328	31 29 36 31 32 34 32 33 34 30	21 21 20 21 27 24 22 23 16	88 81 114 82 72 74 72 74 72 82 82	392 403 386 393 390 405 394 431	635 617 595 529 607 624 614 670	20 19 25 20 27 24 20 18	697.8935588 667.8299886 802.1218015 665.8704169 706.1178887 696.6029669 660.2330244 695.517572	-62.89 -50.82 -207.1 -136.8 -99.11 -72.60 -46.23 -25.51
150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165	0.98845 0.97787 0.98746 0.9901 0.78596 0.76556 0.5735 0.98501 0.95664 0.76112 0.30963 0.98513 0.98564 0.66688 0.66024	0.00834 0.01716 0.00987 0.00715 0.00787 0.00796 0.01096 0.01204 0.00936 0.00936 0.00934 0.00834 0.00834	0.00322 0.00463 0.00267 0.00276 0.00303 0.00307 0.00287 0.00288 0.00296 0.00281 0.00294 0.00294	0.05955 0.06862 0.0395 0.05104 0.0562 0.01819 0.01703 0.05482 0.06129 0.04159	0.00357 0.00515 0.00296 0.00306 0.00337 0.00341 0.00319 0.00253 0.00328	36 31 32 34 32 33 33 34 30	20 21 27 24 22 23 16	114 82 72 74 72 82	386 393 390 405 394	595 529 607 624 614	25 20 27 24 20	802.1218015 665.8704169 706.1178887 696.6029669 660.2330244	-207.1 -136.8 -99.11 -72.60 -46.23
151 152 153 154 155 156 157 158 159 160 161 162 163 164 165	0.97787 0.98746 0.9891 0.70479 0.75556 0.5735 0.98501 0.95664 0.76112 0.30963 0.98517 0.66688 0.60024	0.01716 0.00987 0.00715 0.00787 0.00796 0.00745 0.01096 0.01204 0.00936 0.00761 0.00834 0.00753	0.00463 0.00267 0.00276 0.00303 0.00307 0.00287 0.00228 0.00296 0.00281 0.00294 0.00294 0.00322	0.06862 0.0395 0.05104 0.0562 0.01819 0.01703 0.05482 0.06129 0.04159	0.00515 0.00296 0.00306 0.00337 0.00341 0.00319 0.00253 0.00328	31 32 34 32 33 33 34 30	21 27 24 22 23 16	82 72 74 72 82	393 390 405 394	529 607 624 614	20 27 24 20	665.8704169 706.1178887 696.6029669 660.2330244	-136.8 -99.11 -72.60 -46.23
152 153 154 155 156 157 158 159 160 161 162 163 164 165	0.98746 0.9901 0.9891 0.70479 0.75556 0.5735 0.95664 0.76112 0.30963 0.39563 0.98517 0.66688 0.60024	0.00987 0.00715 0.00787 0.00796 0.00745 0.01096 0.01204 0.00936 0.00761 0.00834 0.00191 0.00753	0.00267 0.00276 0.00303 0.00307 0.00287 0.00228 0.00296 0.00281 0.00294 0.00294	0.0395 0.05104 0.0562 0.01819 0.01703 0.05482 0.06129 0.04159	0.00296 0.00306 0.00337 0.00341 0.00319 0.00253 0.00328	32 34 32 33 34 30	27 24 22 23 16	72 74 72 82	390 405 394	607 624 614	27 24 20	706.1178887 696.6029669 660.2330244	-99.11 -72.60 -46.23
153 154 155 156 157 158 159 160 161 162 163 164 165	0.9901 0.9891 0.70479 0.75556 0.5735 0.98501 0.95664 0.76112 0.30963 0.98517 0.66688 0.60024	0.00715 0.00787 0.00796 0.00745 0.01096 0.01204 0.00936 0.00761 0.00834 0.01191 0.00753	0.00276 0.00303 0.00307 0.00287 0.00228 0.00296 0.00281 0.00294 0.00294	0.05104 0.0562 0.01819 0.01703 0.05482 0.06129 0.04159	0.00306 0.00337 0.00341 0.00319 0.00253 0.00328	34 32 33 34 30	24 22 23 16	74 72 82	405 394	624 614	24 20	696.6029669 660.2330244	-72.60 -46.23
154 155 156 157 158 159 160 161 162 163 164 165	0.9891 0.70479 0.75556 0.5735 0.98501 0.95664 0.76112 0.30963 0.98517 0.66688 0.60024	0.00787 0.00796 0.00745 0.01096 0.01204 0.00936 0.00761 0.00834 0.01191 0.00753	0.00303 0.00307 0.00287 0.00228 0.00296 0.00296 0.00281 0.00294 0.00322	0.0562 0.01819 0.01703 0.05482 0.06129 0.04159	0.00337 0.00341 0.00319 0.00253 0.00328	32 33 34 30	22 23 16	72 82	394	614	20	660.2330244	-46.23
155 156 157 158 159 160 161 162 163 164 165	0.70479 0.75556 0.5735 0.98501 0.95664 0.76112 0.30963 0.98517 0.66688 0.60024	0.00796 0.00745 0.01096 0.01204 0.00936 0.00761 0.00834 0.01191 0.00753	0.00307 0.00287 0.00228 0.00296 0.00281 0.00294 0.00322	0.01819 0.01703 0.05482 0.06129 0.04159	0.00341 0.00319 0.00253 0.00328	33 34 30	23 16	82					
156 157 158 159 160 161 162 163 164 165	0.75556 0.5735 0.98501 0.95664 0.76112 0.30963 0.98517 0.66688 0.60024	0.00745 0.01096 0.01204 0.00936 0.00761 0.00834 0.01191 0.00753	0.00287 0.00228 0.00296 0.00281 0.00294 0.00322	0.01703 0.05482 0.06129 0.04159	0.00319 0.00253 0.00328	34 30	16		431	670	18		
157 158 159 160 161 162 163 164 165	0.5735 0.98501 0.95664 0.76112 0.30963 0.98517 0.66688 0.60024	0.01096 0.01204 0.00936 0.00761 0.00834 0.01191 0.00753	0.00228 0.00296 0.00281 0.00294 0.00322	0.05482 0.06129 0.04159	0.00253	30			437	686	20	632,8948003	53.10
158 159 160 161 162 163 164 165	0.98501 0.95664 0.76112 0.30963 0.98517 0.66688 0.60024	0.01204 0.00936 0.00761 0.00834 0.01191 0.00753	0.00296 0.00281 0.00294 0.00322	0.06129 0.04159	0.00328		22	76	374	602	20	632.6948003	-26.60
159 160 161 162 163 164 165	0.95664 0.76112 0.30963 0.98517 0.66688 0.60024	0.00936 0.00761 0.00834 0.01191 0.00753	0.00281 0.00294 0.00322	0.04159		31	19	77	381	602	20	632,7053218	-29.70
160 161 162 163 164 165	0.76112 0.30963 0.98517 0.66688 0.60024	0.00761 0.00834 0.01191 0.00753	0.00294 0.00322		0.00312	29	22	81	432	642	18	674.0443943	-32.04
161 162 163 164 165	0.30963 0.98517 0.66688 0.60024	0.00834 0.01191 0.00753	0.00322			34	23	86	461	743	17	714.8091357	28.15
162 163 164 165	0.98517 0.66688 0.60024	0.01191 0.00753		0.05359	0	32	19	23	409	643	20	421.1651402	221.8
163 164 165	0.60024		0.00292		0.00325	30	22	92	362	581	22	710.3872401	-129.3
165			0.0029	0.05378	0.00323	29	18	87	394	627	23	639,1636597	-12.10
	0.0500	0.00934	0.0036	0.04402	0.004	24	17	76	400	615	19	566.2455492	48.75
166	0.8588	0.0071	0.0027	0.0404	0.003	30	22	75	430	686	18	655,9860106	30.01
	0.9691	0.0073	0.0028	0.0417	0.0031	37	23	75	438	667	19	702.398965	-35.3
167	0.9677	0.0076	0.0029	0.0435	0.0033	32	25	79	468	755	16	714,9036591	40.05
168	0.9368	0		0.2342		32	15	80	479	717	15	910.6185599	-193.0
169	0.98787	0.00875		0.06252		29	ung 20	1110	ensile	778	1gui.	643,7299513	134.
169	0.9903	0.00875	0.00338	0.06252	0.00375	34	20	71	406	687	1/	677,9940633	9.005
													51.99
171	0.9891	0.00787	0.00303	0.03934	0.00337	27	19	72	410	663	19	611.0051832	
172	0.98934	0.00769	0.00297	0.04397	0.0033	26	22	75	455	707	17	646.8676037	60.1
173	0.73551	0.00686	0.00265		0.00294	28	23	72	513	778	16	639.5045253	138.4
174	0.97761	0.00796	0.00307	0.04547	0.00341	33	24	77	462	666	16	702.4259177	-36.4
175	0.9901	0.00715	0.00276	0.05104	0.00306	30	21	73	459	698	17	646.1049161	51.89
176	0.98979	0.00722	0.00278	0.05155	0.00309	32	23	73	433	656	20	674.544061	-18.5
177	0.986	0.01	0.004	0.05716	0.00429	28	17	68	420	691	20	579.1999397	111.8
178	0.9886	0.00814	0.00326	0.04652		30	17	74	448	697	17	610.2561721	86.74
179	0.97914	0.0149	0.00596	0.08514	0.00639	28	19	92	364	553	22	677.8129226	-124.0
	0.98383	0.01167	0.0045	0.0667	0.005	34	20	82	419	634	19	680.5606407	-46.5
180	0.98934	0.00769	0.00297	0.05496	0.0033	32	20	73	397	681	22	643.8079205	37.19
180 181		0.00707	0.00143	0.05629	0.00338	23	18	64	479	762	17	544.1643585	217.8
	0.99069	0.00788	0.00377	0.05385	0.00404	34	15	103	374	639	22	675.6382396	-36.6
181		0.00788				32							
181 182	0.99069 0.6462		0.0058	0.06214	0.00621		23	97	425	661	19	740.9671423	-79.96
181 182 183	0.99069 0.6462 0.97349	0.01346		0.06214	0.00621	29	23	97 83	425 426	661 660	19 19	740.9671423 661.4643918	
181 182 183 184	0.99069 0.6462 0.97349	0.01346 0.02071	0.0058										-79.96 -1.464 66.90

 188
 0.7956
 0.0101
 0.0027
 0.0403
 0.003
 29
 21
 76
 443
 747
 18
 53.4897559
 112.5152

 189
 0.667
 0.0111
 0.0035
 0.0043
 33
 27
 83
 433
 727
 17
 73.44901
 -3.44901

 Figure (17-m) Testing the prediction model and calculating the mean

			e	rror	in pr	edic	ting	the t	ensile	stre	ngth.		
190	0.93306	0.00976	0.00293	0.0434	0.00325	39	21	87	423	672	19	724.9590273	-52.95903
191	0.77837	0.00841	0.00284	0.04207	0.00316	30	17	73	402	605	19	591.018618	13.98138
192	0.98979	0.00737	0.00284	0.04212	0.00316	33	20	77	433	726	18	663.5611413	62.43886
193	0.98968	0.00745	0.00287	0.04257	0.00319	30	24	81	444	606	17	704.9184526	-98.91845
194	0.98796	0.00926	0.00278	0.04116	0.00309	30	22	72	437	703	18	649.1640521	53.83595
195	0.7475	0.00769	0.00297	0.04397	0.0033	30	17	82	448	744	17	622.2687546	121.7312
196	0	0.02595	0.01001	0.18539	0.01112	31	27	88	378	610	21	677.7939577	-67.79396
197	0	0.03186	0.01229	0.22758	0.01365	30	16	76	433	787	18	514.6043996	272.3956

Average Prediction Error 4.750072

Figure (17-n) Testing the prediction model and calculating the mean

error in predicting the tensile strength. From Figure (17) the tensile strength prediction process was performed for 197 samples and the mean error was very small 2.928656 compared to the sample size 197 and the mean error sign was positive and this indicates that the real value is greater than the prediction value, so we increased the mean error to the prediction to get On average error equal to zero.

3.4. Testing the Elongation Ratio Prediction Model:

Test the prediction model and calculate the average error in the prediction of the elongation ratio, and these results are shown in Figure (18) for all 198 samples obtained from the prediction model.

NO	0.01	C. 14.	F-01	Line	Del	0	01		Yield	Tensile		Expected Yi	eld Erro
NO	DRI	FeMn	FeSi	Lime	Dol.	С	Si	Mn	Effort	Strength	Elongation		
1	0.93647	0.00745	0.00287	0.04363	0.00319	34	23	81	448	747	20	21.0726868	-1.072687
2	0.93779	0.00729	0.00281	0.04897	0.00313	31	19	75	429	668	17	20.10764223	-3.107642
3	0.66688	0.00729	0.00281	0.04168	0.00313	30	20	74	431	681	18	18.00718119	-0.007181
4	0.93579	0.00753	0.0029	0.0484	0.00323	32	21	70	450	673	21	19.73806845	1.261932
5	0.95863	0.00729	0.00281	0.0521	0.00313	30	22	72	475	771	15	19.84661656	-4.846617
6	0.9244	0.00886	0.00342	0.05065	0.0038	30	19	80	384	619	20	20.41210911	-0.412109
7	0.93579	0.00753	0.0029	0.04302	0.00323	31	18	77	412	653	19	20.11550498	-1.115505
8	0.59473	0.04248	0.02294	0.08496	0	29	22	76	457	700	16	16.75249696	-0.752497
9	0.84966	0.00959	0.0037	0.05482	0	32	21	75	382	583	26	21.2423502	4.75765
10	0.9289	0.00834	0.00322	0.05955	0.00357	29	23	79	452	732	16	20.44155049	-4.44155
11	0.75023	0.007	0.0027	0.05002	0.003	33	24	70	428	692	17	18.87059557	-1.870596
12	0.8651	0.00631	0.00243	0.03514	0.0027	30	26	74	442	717	20	18.98196027	1.01804
13	0.94875	0.00722	0.00278	0.04125	0.00309	32	25	76	419	650	19	20.21238904	-1.212389
14	0.94087	0.00693	0.00267	0.04457	0.00297	35	18	74	442	712	22	20.58348869	1.416511
15	0.69409	0.00715	0.00276	0.0347	0.00306	33	26	70	444	729	17	18.06562174	-1.065622
16	0.9329	0.00787	0.00303	0.0562	0.00337	34	23	72	394	651	20	20.51422383	-0.514224
17	0.8904	0.00769	0.00297	0.05496	0.0033	34	21	74	370	613	21	20.43073524	0.569265
18	0.8835	0.0091	0.0035	0.0455	0.0039	32	19	68	412	622	21	19.12450461	1.875495
19	0.917	0.0073	0.0028	0.0427	0.0031	31	22	71	408	673	25	19.38161619	5.618384
20	0.9471	0.0074	0.0029	0.0138	0.0032	31	22	72	418	653	18	18.76762279	-0.767623
21	0.9391	0.0071	0.0028	0.0143	0.0031	32	21	75	437	697	17	19.21726595	-2.217266

Figure (18-a) Testing the prediction model and calculating the mean

			e	rror i	in pre	edic	ting 1	the e	longa	tion	ratio.		
22	0.91695	0.00729	0.00281	0.01563	0.00313	31	21	70	394	639	20	18.44029118	1.559709
23	0.60376	0.01208	0.00466	0.05175	0.00518	29	21	86	433	655	26	18.98059515	7.019405
24	0.98945	0.00761	0.00294	0.02936	0.00326	31	20	77	374	564	21	20.00962497	0.990375
25	0.98957	0.00753	0.0029	0.03012	0.00323	35	25	75	410	658	20	20.52592265	-0.525923
26	0.65127	0.01018	0.00275	0.05495	0.00305	34	14	72	387	595	22	20.62189811	1.378102
27	0.96618	0.02196	0.01186	0.24155	0.01318	37	18	66	379	593	21	21.03074562	-0.030746
28	0.9711	0.00819	0.00316	0.0585	0.00351	30	19	69	370	554	26	19.80448282	6.195517
29	0.93779	0.00729	0.00281	0.04168	0.00313	35	21	74	388	609	20	20.4752151	-0.475215
30	0.93594	0.0113	0.00436	0.04841	0.00484	35	25	73	380	626	20	20.55082091	-0.550821
31	0.98802	0.00865	0.00333	0.0457	0.00371	25	11	66	365	546	24	18.32579155	5.674208
32	0.98989	0.00729	0.00281	0.0521	0.00313	32	20	74	403	651	19	20.58329295	-1.583293
33	0.95683	0.00761	0.00294	0.05437	0.00326	29	18	81	399	597	18	20.65331924	-2.653319
34	0.98934	0.00769	0.00297	0.05496	0.0033	35	14	75	409	676	16	21.28841077	-5.288411
35	0.78927	0.01036	0.00266	0.04933	0.00296	34	19	77	376	608	21	22.01564244	-1.015642
36	0.73921	0.00761	0.00315	0.04348	0.00326	31	15	98	358	559	22	20.86484841	1.135152
37	0.98958	0.00729	0.00313	0.04167	0.00313	43	15	73	401	633	21	21.69275521	-0.692755
38	0.70409	0.00761	0.00285	0.04757	0.00285	26	23	62	444	627	16	16.70872873	-0.708729
39	0.9861	0.0105	0.0034	0.0479	0.0029	26	18	68	343	537	23	20.12662535	2.873375
40	0.9717	0.0223	0.0061	0.081	0.0061	25	18	75	393	573	24	24.28867697	-0.288677
41	0.3457	0.0296	0.0074	0.0741	0.0074	28	17	78	371	556	22	23.55087287	-1.550873
42	0.9864	0.0099	0.0037	0.0493	0.0037	24	12	98	406	660	19	21.82946211	-2.829462

Use of Multiple Linear Regression Technology in Controlling the Technical Specifications of Industrial Products.

Figure (18-b) Testing the prediction model and calculating the mean

43 44 45 46			e	rror :	ın pr	edict	ing	tne e		non	гапо.		
44 45	0.70323	0.01125	0.00422	0.07032	0.00422	33	18	1.01	1011ga	681	26	12.44998076	13.5500
	0.98806	0.00869	0.00326	0.04886	0.00326	35	16	87	400	626	20	22.57936808	-2.57936
	0.68985	0.01054	0.00259	0.04791 0.05373	0.00287	38	2 24	84	426	664 542	18 23	23.01836118 19.22144224	-5.01836
47	0.98684	0.00987	0.00329	0.05482	0.00329	36	19	84	326	499	25	23.27503851	1.72496
48	0.97959	0.01633	0.00408	0.06803	0.00408	33	17	109	366	565 584	22 22	28.31119542 29.03999786	-6.31119
50	0.96691	0.00859	0.00301	0.05372	0.00322	24	26	76	348	537	22	19.61628068	2.38371
51	0.98253	0.01365	0.00382	0.05459	0.00328	37	21	87	385	608	23	25.33175211	-2.33175
52 53	0.97986	0.01633	0.00381	0.05444	0.00327	33	18	91 90	397 411	598 626	20 23	26.63076635 22.03150127	-6.63076
54	0.98446	0.01244	0.00311	0.05181	0.00311	32	24	79	405	636	19	23.75433096	-4.75433
55	0.98446	0.01244 0.01007	0.00311	0.05181	0.00311	38	22	78	392 384	630 619	20 20	24.69370392 23.94680492	-4.69370
57	0.9838	0.01007	0.00347	0.05787	0.00302	38	10	89	413	679	25	25.63040451	-0.63040
58	0.98542	0.01106	0.00352	0.06033	0.00302	29	14	88	397	633	20	23.14791782	-3.14791
59 60	0.98571	0.01084	0.00345	0.04929	0.00296	36	20	82	376	591 632	27 25	23.3832583 26.45511118	3.61674
61	0.9821	0.0149	0.0031	0.0595	0.0032	28	17	97	329	500	25	26.77857054	-1.40011
62	0.8673	0.0071	0.0031	0.0561	0.0031	35	20	101	424	637	20	22.91362101	-2.91362
63	0.7668	0.0124	0.0031	0.0518	0.0031	38	21	81	429	629	19	23.71723463	-4.71723
Fig	ure (1	18-c							del ar longa			ting the i	mean
64	0.9768	0.01954		0.06105		33	18	110 C	390	631	20	28.76485953	-8.7648
65	0.97622				0.00375	33	18	81	409	645	24	27.93275239	-3.93275
66	0.98874					35	29	83	417	652	18	21.57459426	-3.57455
67 68		0.01365	0.00328	0.05461	0.00328	28 32	21 11	80	381 380	566 578	22 22	23.70640527 28.18587802	-1.70640 -6.18587
69	0.78254				0.00247	35	21	97	407	610	20	23.5692309	-3.56923
70		0.01332		0.05123	0.00307	35	18	92	422	650	19	24.89232214	-5.8923
71	0.79523			0.0497	0.00298	34	21	89	413	627	19	24.42587611	-5.4258
72 73	0.72131 0.9865			0.05464	0.00328	31 33	20	89 96	399 429	594 680	21 19	23.28599584 24.46184061	-2.2859 -5.4618
74	0.63102	0.01283	0.00321	0.05348	0.00321	24	19	72	415	628	20	19.69447356	0.30552
75	0.73892				0.00296	33	13	96	411	629	20	24.01069441	-4.0106
76 77	0.98305	0.01356	0.00339	0.0678	0.00339	34 33	22	110 92	438 415	730 696	17 19	28.010949 24.30999215	-11.010
78		0.01387	0.00347	0.05/8	0.00347	31	1/	92	415 359	696 545	19 22	24.30999215 24.43949952	-5.3099
79	0.72821	0.01231	0.00308	0.05128	0.00308	30	111	100	429	663	20	24.03953419	-4.0395
80	0.55894				0.00305	36	19	94	413	655	19	22.79286743	-3.79286
81 82		0.0079	0.003	0.0495	0.003	33	17 19	92 79	413 401	633 643	20	22.75111734	-2.75111
82			0.003		0 0031	29 38	19	79	401	643 635	19 19	21.14508478 22.05740572	-2.14508
84		0.0073		0.0417	0.0001	32	12	66	433	668	19	19.60757062	-0.60757
Fig	ure (1	18-d				predi	ictio	n mo			lcula	ting the i	
0	,			-					longa			0	
85 86		0.00869	0.00326	0.04343	0.00326	33	25	79 83	386	566	22	19.90021039	2.09979
85		0.01085	0.00266	0.04932	0.01365	30	20	83	412 364	611 557	19 23	24.33623292 25.61530745	-5.33623
88	0.98934	0.00769	0.00297	0.05496	0.0033	31	22	81	383	657	20	21.21226846	-1.21226
89			0.00287	0.05321	0.00319	28	24	84	494	535	20	20.94862796	-0.94862
90 91		0.001178	0.00289	0.04284	0.00321 0.00316	34	21	81	380	603 738	20 18	23.87230979 20.99945266	-3.87231
92		0.01204	0.00328	0.04376	0.00328	33	20	92	413	657	21	24.51429094	-3.51429
93 94	0.93458	0.0113	0.00277	0.05135	0.00308	36	18	78	384	601 586	20 20	23.77198414 23.4668759	-3.77198
94		0.01166	0.00286	0.05298	0.00318	30	15	81 83	376	599	20	23.8462765	-3.46687
96													
		0.00729	0.00281	0.0521	0.00313	32	23	81	400	702	19	19.64301716	
97	0.98979	0.00729	0.00292	0.05209	0.00313	32	19	76	400 369	623	21	20.66309485	0.33690
	0.98979								400				0.33690
97 98 99 100	0.98979 0.9009 0.98413 0.98462	0.00729 0.07207 0.0127 0.01231	0.00292 0.02703 0.00317 0.00308	0.05209 0.22523 0.05291 0.05231	0.00313 0.02703 0.00317 0.00308	32 36 36 34	19 22 17 20	76 82 85 77	400 369 400 374 418	623 602 578 645	21 19 26 19	20.66309485 28.75380658 25.15128434 23.88403608	0.336908 -9.75380 0.848718 -4.88403
97 98 99 100 101	0.98979 0.9009 0.98413 0.98462 0.9867	0.00729 0.07207 0.0127 0.01231 0.00998	0.00292 0.02703 0.00317 0.00308 0.00333	0.05209 0.22523 0.05291 0.05231 0.05543	0.00313 0.02703 0.00317 0.00308 0.00333	32 36 36 34 31	19 22 17 20 22	76 82 85 77 87	400 369 400 374 418 431	623 602 578 645 673	21 19 26 19 21	20.66309485 28.75380658 25.15128434 23.88403608 22.74274858	-0.64301 0.33690 -9.75380 0.848716 -4.88403 -1.74274
97 98 99 100	0.98979 0.9009 0.98413 0.98462 0.9867 0.6483	0.00729 0.07207 0.0127 0.01231	0.00292 0.02703 0.00317 0.00308	0.05209 0.22523 0.05291 0.05231 0.05543	0.00313 0.02703 0.00317 0.00308	32 36 36 34	19 22 17 20	76 82 85 77	400 369 400 374 418	623 602 578 645	21 19 26 19	20.66309485 28.75380658 25.15128434 23.88403608	0.33690 -9.75380 0.848711 -4.88403
97 98 99 100 101 102 103 104	0.98979 0.9009 0.98413 0.98462 0.9867 0.6483 0.973 0.9787	0.00729 0.07207 0.0127 0.01231 0.00998 0.0093 0.0189 0.017	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0081 0.0043	0.05209 0.22523 0.05291 0.05231 0.05543 0.05543 0.0525 0.0811 0.0709	0.00313 0.02703 0.00317 0.00308 0.00333 0.0031 0.0081 0.0043	32 36 34 31 34 31 34 31 22	19 22 17 20 22 25 17 17	76 82 85 77 87 87 80 70 64	400 369 400 374 418 431 372 425 390	623 602 578 645 673 580 650 542	21 19 26 19 21 21 17 26	20.66309485 28.75380658 25.15128434 23.88403608 22.74274858 20.76458491 19.76676447 22.01184122	0.33690 -9.75380 0.848711 -4.88403 -1.74274 0.235411 -2.76676 3.988151
97 98 99 100 101 102 103 104 105	0.98979 0.9009 0.98413 0.98462 0.9867 0.6483 0.973 0.9787 0.7095	0.00729 0.07207 0.0127 0.01231 0.00998 0.0093 0.0189 0.017 0.008	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0081 0.0043 0.0027	0.05209 0.22523 0.05291 0.05231 0.05543 0.0555 0.0811 0.0709 0.05	0.00313 0.02703 0.00317 0.00308 0.00333 0.0031 0.0081 0.0043 0.003	32 36 36 34 31 34 31 22 29	19 22 17 20 22 25 17 17 17 22	76 82 85 77 87 80 70 64 92	400 369 400 374 418 431 372 425 390 419	623 602 578 645 673 580 650 542 654	21 19 26 19 21 21 17 26 19	20.66309485 28.75380658 25.15128434 23.88403608 22.74274858 20.76458491 19.76676447 22.01184122 20.78353886	0.33690 -9.75380 0.84871 -4.88403 -1.74274 0.23541 -2.76676 3.98815 -1.78353
97 98 99 100 101 102 103 104 105	0.98979 0.9009 0.98413 0.98462 0.9867 0.6483 0.973 0.9787 0.7095	0.00729 0.07207 0.0127 0.01231 0.00998 0.0093 0.0189 0.017 0.008	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0081 0.0043 0.0027) Tes	0.05209 0.22523 0.05291 0.05231 0.05543 0.0525 0.0811 0.0709 0.05 sting	0.00313 0.02703 0.00317 0.00308 0.00333 0.0031 0.0081 0.0043 0.003 the	32 36 36 34 31 34 31 22 29 predi	19 22 17 20 22 25 17 17 22 17 22 17 17 22	76 82 85 77 87 80 70 64 92 n mO	400 369 400 374 411 372 425 390 419 odel ar	623 602 578 645 673 580 650 542 654 654 1d ca	21 19 26 19 21 21 17 26 19 Icula	20.66309485 28.75380658 25.15128434 23.88403608 22.74274858 20.76458491 19.76676447 22.01184122	0.33690 -9.75380 0.84871 -4.88403 -1.74274 0.23541 -2.76676 3.98815 -1.78353
97 98 99 100 101 102 103 104 105	0.98979 0.9009 0.98413 0.98462 0.9867 0.6483 0.973 0.9787 0.7095 ure (1	0.00729 0.07207 0.0127 0.01231 0.00998 0.0093 0.0189 0.017 0.008	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0081 0.0043 0.0027) Tes	0.05209 0.22523 0.05291 0.05231 0.05543 0.0525 0.0811 0.0709 0.05 sting	0.00313 0.02703 0.00317 0.00308 0.00333 0.0031 0.0081 0.0043 0.003 the j	32 36 36 34 31 34 31 22 29 predi	19 22 17 20 22 25 17 17 22 17 22 17 17 22	76 82 85 77 87 80 70 64 92 n mO	400 369 400 374 418 431 372 425 390 419	623 602 578 645 673 580 650 542 654 654 1d ca	21 19 26 19 21 21 17 26 19 Icula	20.66309485 28.75380658 25.15128434 23.88403608 22.74274858 20.76458491 19.76676447 22.01184122 20.78353886	0.33690 -9.75380 0.848711 -4.88403 -1.74274 0.235411 -2.76676 3.98815 -1.78353
97 98 99 100 101 102 103 104 105 Fig	0.98979 0.9009 0.98492 0.98462 0.9867 0.6483 0.973 0.9787 0.7095 ure (1	0.00729 0.07207 0.0127 0.01231 0.00938 0.0129 0.017 0.008 18-e	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0081 0.0043 0.0027) Tes 0.00273 0.00265	0.05209 0.22523 0.05291 0.05231 0.05543 0.0525 0.0811 0.0709 0.05 Sting 0.05 Sting 0.04038 0.04903	0.00313 0.02703 0.00317 0.00308 0.0033 0.0031 0.0081 0.0043 0.003 the j 0.00303 0.00303 0.00303	32 36 36 34 31 22 29 predi edict 31 31	19 22 17 20 22 25 17 17 22 17 17 22 17 17 22 17 17 22 17 20 20 21	76 82 85 77 80 70 64 92 n mo the e	400 369 400 374 418 431 372 425 390 419 odel ar longa 430 414	623 602 578 645 673 580 650 542 654 nd ca tion 678 641	21 19 26 19 21 21 17 26 19 10 10 10 10 19	20.66309485 28.75306658 25.15128434 23.88403508 22.74274858 20.76458491 19.76676447 22.01784122 20.73351865 ting the 1 20.83042377 20.33941389	0.33690 -9.75380 0.84871 -4.88403 -1.74274 0.23541 -2.76676 3.98815 -1.78353 mean
97 98 99 100 101 102 103 104 105 Fig	0.98979 0.9009 0.98413 0.98462 0.98467 0.6483 0.973 0.9787 0.7095 ure (1 0.94145 0.9901	0.00729 0.07207 0.0127 0.01231 0.00938 0.0093 0.0189 0.017 0.008 8-e	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0083 0.0027) Tes 0.00273 0.0026 0.0029	0.05209 0.22523 0.05291 0.05231 0.05543 0.0555 0.0811 0.0709 0.05 Sting 0.04038 0.04038 0.04038	0.00313 0.02703 0.00317 0.00308 0.00333 0.0031 0.00843 0.003 the j 0.00303 0.00254 0.0033	32 36 36 34 31 34 31 22 29 predi edict 31 31 33	19 22 17 20 22 25 17 17 22 25 17 17 22 17 17 22 17 17 22 17 20 21 21	76 82 85 77 80 70 64 92 n mO the e 77 77 84	400 369 400 374 418 431 372 425 390 419 odel ar longa 430 414 331	623 602 578 645 673 580 650 542 654 664 1d ca tion 678 641 677	21 19 26 19 21 21 21 17 26 19 19 10 20	20.65399455 28.75380658 25.15124434 23.88403608 22.74274858 20.76458491 19.76676447 22.01784472 20.78353886 ting the 1 20.83042377 20.33941389 21.48332567	0.33690 -9.75380 0.84871 -4.84400 -1.74274 0.23541 -2.76676 3.99815 -1.78353 MCCAN -0.83042 -1.33941 -1.48332
97 98 99 100 101 102 103 104 105 Fig	0.98979 0.9009 0.98413 0.98442 0.98452 0.9867 0.6483 0.973 0.9787 0.7095 ure (1 0.94145 0.996901 0.98999	0.00729 0.07207 0.0127 0.01231 0.00938 0.0129 0.017 0.008 18-e	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0081 0.0043 0.0027) Tes 0.00273 0.00265	0.05209 0.22523 0.05291 0.05231 0.05543 0.0525 0.0811 0.0709 0.05 Sting 0.05 Sting 0.04038 0.04903	0.00313 0.02703 0.00317 0.00308 0.0033 0.0031 0.0081 0.0043 0.003 the j 0.00303 0.00303 0.00303	32 36 36 34 31 22 29 predi edict 31 31	19 22 17 20 22 25 17 17 22 17 17 22 17 17 22 17 17 22 17 20 20 21	76 82 85 77 80 70 64 92 n mo the e	400 369 400 374 418 431 372 425 390 419 odel ar longa 430 414	623 602 578 645 673 580 650 542 654 nd ca tion 678 641	21 19 26 19 21 21 17 26 19 10 10 10 10 19	20.66309485 28.75306658 25.15128434 23.88403508 22.74274858 20.76458491 19.76676447 22.01784122 20.73351865 ting the 1 20.83042377 20.33941389	0.33690 -9.75380 0.84871 -4.88400 -1.74274 0.23541 -2.76676 3.98815 -1.78353 THE ANNO -0.83042 -1.33941 -1.48322 -3.379036
97 98 99 100 101 102 103 104 105 Fig 106 107 108 109 110 111	0.98379 0.9009 0.98413 0.98452 0.9867 0.6483 0.9787 0.7095 ure (] 0.96901 0.94145 0.9901 0.94145 0.9901 0.94145 0.9901 0.94145	0.00729 0.07207 0.0127 0.01231 0.00938 0.0093 0.0189 0.017 0.008 I.S-e 0.00808 0.00686 0.007 0.00682 0.00822 0.01387	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0081 0.0043 0.0027) Tes 0.0027 0.00273 0.00265 0.0029 0.00281 0.00317	0.05209 0.22523 0.05291 0.05251 0.05543 0.05543 0.05543 0.05543 0.05543 0.0505 0.0811 0.0709 0.05 0.05 0.04038 0.04038 0.04903 0.05001 0.0521 0.05205	0.00313 0.02703 0.003017 0.003033 0.00313 0.0031 0.0043 0.003 the j 0.00303 the j 0.00303 0.00294 0.00313 0.00313 0.00312	32 36 34 31 34 31 22 29 predi edict 31 31 33 41 32 30	19 22 17 20 22 25 17 17 22 17 22 17 20 21 20 21 20 21 20 21 20 21 20	76 82 85 77 87 80 70 64 92 n mo the e 77 77 84 90 70 84	400 359 400 374 418 431 372 425 390 419 del ar 10nga 430 414 391 395 410 386	623 602 578 645 673 580 650 542 654 cos tion 678 641 677 644 698 605	21 19 26 19 21 21 17 25 19 Icula ratio. 20 20 20 19 20 20 19 23	20.65/30445 28.7530658 25.15128434 23.840568 22.74274858 20.7645849 19.767545447 22.01184122 20.7355886 ting the 1 20.83042277 20.33941389 21.44332567 23.7903639 20.22210252	0.33690: -9.75380 0.848711 -8.8403 -1.74274 0.235411 -2.76676 3.98615 -1.78353 mean -0.83042 -1.33941 -1.48332 -3.79036 -1.22210 -1.12798
97 98 99 100 101 102 103 104 105 Fig 106 107 108 109 110 111 111 112	0.98379 0.9009 0.98413 0.98462 0.98452 0.9843 0.9787 0.7095 ure (1 0.96901 0.94145 0.9899 0.98999 0.95734 0.93842 0.93642	0.00729 0.07207 0.01231 0.00938 0.0093 0.0189 0.017 0.008 [8-e]	0.00292 0.02703 0.00317 0.00303 0.00333 0.0028 0.0043 0.0027 0.00275 0.00273 0.00228 0.0029 0.00281 0.00281 0.00312 0.00312	0.05209 0.22523 0.05291 0.05251 0.05543 0.05543 0.0555 0.0811 0.0709 0.05 5005 5005 5005 0.04038 0.04903 0.05001 0.0521 0.0523 0.0678 0.04738	0.00313 0.02703 0.00317 0.00303 0.00333 0.0031 0.0043 0.003 the j 0.00303 0.00254 0.00303 0.00254 0.00313 0.00312 0.00315	32 36 36 34 31 32 29 predi 31 31 33 41 32 30 39	19 22 17 20 22 25 17 17 22 17 22 17 17 22 17 17 22 17 20 21 21 21 20 21 21 20 21 21 20 21 22 25 25 22 25 25 22 25 25 22 25 25 22 25 22 22	76 82 85 77 87 80 70 64 92 n mC the e 77 77 77 84 90 70 84 90	400 369 400 374 411 372 425 390 419 odel ar longa 410 395 410 395 410 395 401	623 602 578 645 650 542 654 0542 654 0542 654 056 641 677 644 698 605 661	21 19 26 19 21 17 26 19 Icula ratio . 20 19 20 19 20 19 20 19	20.65309485 28.7530958 28.7530958 25.15128454 23.8840546 22.74274858 20.76458491 19.76676447 22.0184122 20.735386 ting the 1 20.83042377 20.33941389 21.48332567 23.79036839 20.22210582 24.12799725 23.05174355	0.33690 -9.75380 0.84971 -4.84403 -1.74274 0.23541 -2.76676 3.98815 -1.78353 MCAN -0.83044 -1.33941 -1.43354 -1.23210 -1.22210 -1.22210 -1.22210 -1.22210 -1.22210 -1.22210
97 98 99 100 101 102 103 104 105 Fig 106 107 108 109 110 111	0.98979 0.9009 0.98413 0.98443 0.98462 0.98452 0.973 0.9787 0.7095 ure (1 0.946901 0.94145 0.94767 0.95899 0.95634 0.95344 0.95344 0.95345 0.95447	0.00729 0.07207 0.01231 0.00938 0.0093 0.0189 0.0189 0.017 0.008 [8-e] 0.00686 0.007 0.00686 0.007 0.00682 0.00822 0.01387 0.00737 0.00739	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0041 0.0041 0.0043 0.0027 0.00275 0.00273 0.00281 0.00281 0.00317 0.00281	0.05209 0.22523 0.05251 0.05251 0.05543 0.05543 0.08514 0.0709 0.05 0.0811 0.04038 0.04903 0.05691 0.0521 0.0578 0.0578 0.0578	0.00313 0.02703 0.003017 0.003033 0.00313 0.0031 0.0043 0.003 the j 0.00303 the j 0.00303 0.00294 0.00313 0.00313 0.00312	32 36 34 31 34 31 22 29 predi edict 31 31 33 41 32 30	19 22 17 20 22 25 17 17 22 17 22 17 20 21 20 21 20 21 20 21 20 21 20	76 82 85 77 87 80 70 64 92 n mo the e 77 77 84 90 70 84	400 359 400 374 418 431 372 425 390 419 del ar 10nga 430 414 391 395 410 386	623 602 578 645 673 580 650 542 654 cos tion 678 641 677 644 698 605	21 19 26 19 21 21 17 25 19 Icula ratio. 20 20 20 19 20 20 19 23	20.65/30445 28.7530658 25.15128434 23.840568 22.74274858 20.7645849 19.767545447 22.01184122 20.7355886 ting the 1 20.83042277 20.33941389 21.44332567 23.7903639 20.22210252	0.33690 -9.75390 0.48471 -4.88400 -1.74274 0.23541 -2.76676 3.98815 -1.78353 COMPARIANCE -0.83044 -1.33941 -1.48332 -3.79034 -1.22210 -1.27994 -4.05174 -1.69573 -0.6054
97 98 99 100 101 102 103 104 105 Fig 106 107 108 109 110 111 112 113 114 115	0.98979 0.9009 0.98413 0.98443 0.98462 0.9867 0.6483 0.973 0.7095 UITE (1 0.9737 0.9901 0.9801 0.9801 0.94145 0.9901 0.9801 0.94145 0.9901 0.95734 0.9563 0.95737 0.94563 0.97737 0.97737	0.00729 0.07207 0.01231 0.00938 0.00938 0.0189 0.0189 0.0088 18-e 0.0088 0.00686 0.00686 0.00686 0.0067 0.00729 0.00729 0.00729 0.001377 0.00729	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0081 0.0047 0.00277 0.00273 0.00265 0.0028 0.00281 0.00284 0.00284 0.00281 0.00284	0.05209 0.22523 0.05291 0.05251 0.0525 0.0811 0.0709 0.05 0.0811 0.0709 0.05 0.0801 0.04038 0.04038 0.0503 0.0521 0.0521 0.05203 0.0573 0.04168 0.04168	0.00313 0.02703 0.00317 0.00308 0.00333 0.0031 0.0043 0.0043 0.0043 0.0043 0.0043 0.00303 0.00294 0.00313 0.00312 0.00313 0.00313 0.00313	32 36 34 31 22 29 predi edict a1 31 33 41 32 30 39 36 31 33	19 22 20 22 25 17 17 22 17 17 22 17 17 22 17 20 21 21 20 21 21 20 22 20 22 20 22 22 20 22 22 20 22 22	76 82 85 77 87 80 70 64 92 n mC the e 77 77 77 88 90 70 88 90 70 77 77 77 77 77 77 77 77 77 77	400 389 400 374 411 372 425 390 419 odel ar longa 430 414 391 395 410 385 410 385 410 385 385 410 385 382	623 602 578 645 673 580 650 542 654 10 Ca 654 10 Ca 678 641 677 644 690 661 690 612 606	21 19 26 19 21 17 26 19 17 26 19 20 20 20 20 20 20 20 20 20	20.65309455 28.7530658 28.7530658 23.5452056 23.5452056 23.7427458 20.7645461 19.76676447 22.0180528 20.7645461 19.76676447 22.018053886 tting the 1 20.83042377 20.33941389 21.44332567 23.79036839 20.22210262 23.769376833 20.60994725 23.051764355 20.501764355 20.501764355 20.501764355 20.501764355 20.501764355 20.50176835 20.60994725 20.50176835 20.60994725 20.51118608	0.33690 -9.75390 0.48471 -4.88403 -1.74274 0.23641 -2.76676 3.98815 -1.78353 mean -0.83042 -1.33941 -1.48332 -3.79035 -1.22210 -1.22210 -1.22110
97 98 99 100 101 102 103 104 105 Fig 106 107 108 109 110 111 111 112 113 114 115 116	0.98979 0.5009 0.98413 0.98442 0.98452 0.9857 0.6483 0.973 0.7935 0.7935 0.7955 0.7955 0.7955 0.9899 0.96901 0.98989 0.95734 0.93642 0.93642 0.93734 0.93642 0.93734 0.93642 0.93734 0.93642 0.93734 0.93642 0.93734 0.93642 0.93734 0.93734 0.93734 0.93642 0.93734 0.93737 0.93734 0.93737 0.93734 0.93737 0.93734 0.93734 0.93737 0.93734 0.93734 0.93734 0.93737 0.93734 0.93734 0.93737 0.93734 0.93737 0.93734 0.93737 0.93734 0.93737 0.93747 0.93774 0.93774 0.93774 0.93774 0.93774 0.937774 0.93777777777777777777777777777777777777	0.00729 0.07207 0.01231 0.00938 0.0093 0.0133 0.0189 0.0078 18-e 0.00808 0.00686 0.00686 0.00686 0.00729 0.00729 0.00737 0.00729 0.00737	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0081 0.0027 0.0027 0.00265 0.0029 0.0029 0.00281 0.0029 0.00281 0.00284 0.00284 0.00284 0.00284 0.00284 0.00284	0.05209 0.22523 0.05291 0.05231 0.05543 0.0555 0.08511 0.0709 0.05 0.05 0.04003 0.05001 0.05203 0.0578 0.04738 0.04168 0.05433 0.04161 0.05431	0.00313 0.02703 0.00317 0.00308 0.00333 0.0031 0.0043 0.003 the j 0.00294 0.00312 0.00312 0.00312 0.00313 0.00313 0.00313 0.00313	32 36 34 31 22 29 predict edict 31 31 33 41 32 30 39 36 31 33 33	19 22 25 25 17 17 22 17 17 22 17 17 22 17 17 22 17 20 21 20 21 20 21 20 22 20 22 20 22 23 22 23 24	76 82 85 87 80 70 64 92 n mo the e 77 77 80 70 70 80 80 70 80 83 76 77 80	400 369 400 374 418 421 372 425 390 del ar 419 419 419 419 419 419 419 419 419 414 419 414 419 414 419 414 419 419	623 602 578 645 673 580 650 542 654 1d ca tion 678 641 677 644 698 605 661 690 612 600 6539	21 19 26 19 21 17 26 19 Icula ratio. 20 19 20 20 20 20 20 20 20 20 20 20 20 20 20	20.65309455 28.7530658 28.7530658 23.15128424 23.8840566 22.74274858 20.76454891 19.7667647 22.01194722 20.78353806 ting the 1 20.83042277 20.33941309 21.43322567 21.43322567 22.79038139 20.2221052 24.12798725 20.22110580 20.221052 24.12798725 20.221115800 23.06301454	0.33690 -9.7536 0.4871 -4.88400 -1.74274 0.23541 -2.76676 3.98815 -1.78353 TREAT -0.83044 -1.33944 -1.33944 -1.33944 -1.33944 -1.33944 -1.22210 -
97 98 99 100 101 102 103 104 105 Fig 106 107 108 109 110 111 111 113 114 115 116 117 118	0.98379 0.5009 0.98413 0.98452 0.9887 0.6483 0.973 0.7095 ure (1 0.96901 0.9737 0.9737 0.96902 0.96902 0.96902 0.9737 0.96902 0.96902 0.9737 0.7095 0.97402 0.97737 0.7095 0.96902 0.97737 0.70779 0.96902 0.96902 0.97337 0.70779 0.96902 0.96902 0.97337 0.70179 0.96802 0.96902 0.97337 0.70179 0.96802 0.9737 0.70179 0.96802 0.96802 0.9737 0.70179 0.98682 0.98775 0.98682 0.9975	0.00729 0.07207 0.0127 0.01231 0.00938 0.00939 0.0189 0.00189 0.0088 0.0088 0.00686 0.007 0.00729 0.00737 0.00729 0.00832 0.00137 0.00729 0.00948 0.00848 0.00848 0.00852 0.00125 0.01284 0.01755	0.00292 0.02703 0.00317 0.00308 0.00333 0.0028 0.0028 0.0027 0.0027 0.00265 0.0029 0.0029 0.0029 0.0029 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028	0.05209 0.22523 0.05291 0.05231 0.05543 0.0555 0.0555 0.0555 0.0555 0.0555 0.04038 0.04903 0.05203 0.05203 0.0578 0.04738 0.04168 0.05433 0.04168	0.00313 0.02703 0.00317 0.00308 0.00333 0.0031 0.0043 0.003 the j 0.003 0.00294 0.003 0.00312 0.00313 0.00312 0.00313 0.00312 0.00313 0.00313 0.00312 0.00313 0.00312 0.00313 0.00313	32 36 34 31 22 predi edict 31 32 30 39 36 31 32 30 39 36 31 32 30 33 33 33 33 33 33 33 33 34 34	19 22 25 17 17 22 25 17 17 22 17 17 22 17 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 21 20 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 25 17 17 22 20 20 20 20 20 20 20 20 20 20 20 20	76 82 85 77 80 70 64 92 n mC the e 77 84 90 90 83 76 83 76 83 77 78 84 90 90 83	400 364 400 374 431 431 372 425 390 0del ar 419 419 419 419 419 419 419 419 419 419	623 602 578 645 650 542 654 0542 654 0542 654 0542 654 0542 654 0542 654 651 690 612 690 612 606 539 530 596	21 19 26 19 21 21 21 17 26 19 lcula ratio. 20 20 20 20 20 20 20 20 20 20 20 20 20	20.6509465 20.530656 21.530656 22.1528424 22.1528424 22.1528456 22.1727858 22.1727858 22.074558 20.7455867 20.7455867 20.753586 time the 1 20.753586 time the 1 20.75558 time the	0.33690 -9.75380 0.48471 -4.88403 -1.74274 0.23541 -2.76676 3.98815 -1.78353 THEOREM -0.83042 -1.33944 -1.48332 -3.79030 -1.22210 -1.22910 -1.29100 -1.22910 -1.29100 -1.22910 -1.2910 -1.2910000000 -1
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97 98 99 100 101 102 103 104 105 Fig 100 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124	0.98779 0.9009 0.90413 0.98462 0.98452 0.9787 0.9787 0.9787 0.9787 0.9787 0.9787 0.9787 0.9787 0.9787 0.9951 0.94145 0.94574 0.94575 0.95595 0.95757 0.95595 0.95757 0.95595 0.957570 0.957570 0.957570 0.95757000000000000000000000000000000000	0.00729 0.0127 0.01237 0.01237 0.01231 0.00988 0.00983 0.0187 0.0088 1.8-C 0.00808 0.0086 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0088 1.0087 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00729 1.00719 1.00119 1.00119 1.00119 1.00119 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.00111 1.0	0.00292 0.02703 0.00317 0.00305 0.0028 0.0028 0.0028 0.0027 0.0028 0.00290000000000	0.05209 0.2553 0.05291 0.05231 0.0525 0.0511 0.0525 0.0611 0.0525 0.0611 0.0525 0.0610 0.0525 0.0610 0.0525 0.0610 0.0525 0.0610 0.0553 0.04030 0.0542100000000000000000000000000000000000	0.00313 0.002103 0.00317 0.00330 0.0033 0.0033 0.0033 0.0043 0.0043 0.0031 0.0043 0.0031 0.0031 0.0032 0.00324 0.00315 0.00312 0.00316 0.00316 0.00319 0.00329 0.00329 0.00329 0.00329 0.00329 0.00329	32 36 36 34 31 34 31 22 29 predi 22 30 30 30 30 30 30 30 30 31 33 32 32 32 32 31 33 33 33 33 33 33 33 33 33 33 33 33	19 22 17 20 22 25 17 17 22 25 17 17 22 20 21 21 20 20 21 20 20 20 20 20 22 20 22 23 24 4 18	7 76 82 85 77 87 87 87 70 70 64 92 92 91 mmc the e 777 77 77 77 84 84 90 70 70 70 84 83 70 70 84 83 70 84 88 81 77 81 81 81 77 70 70 70 70 70 70 70 70 70 70 70 70	400 369 374 411 372 425 390 419 odel ar longa 410 395 414 414 391 395 414 417 395 385 401 395 385 401 395 385 385 385 385 385 385 385 385 385 38	633 602 578 645 578 650 650 650 654 654 654 654 654 654 654 654 654 654	21 19 25 19 21 21 21 21 21 21 20 20 20 20 20 20 20 20 20 20 20 20 20	20.6539445 20.530654 21.530654 22.1520644 22.1520654 22.1520654 22.1520654 22.1520654 22.1520654 22.1520654 22.015402 20.1520654 20.15206554 20.15206554 20.15206554 20.15206555	0.33690 9.75360 0.48971 -4.88405 -1.74274 0.23641 -2.76677 3.98815 -1.78355 THE AND -0.83044 -1.33944 -1.48352 -3.79034 -1.22216 -1.12790 -1.22217 -1.45957 -1.22217 -0.60594 -1.22217 -0.60594 -1.22217 -0.60594 -2.30682 -2.30682 -1.46359 -3.20865 -3.2086
97 98 99 100 101 102 103 104 105 Fig 106 107 108 109 110 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123	0.98779 0.9009 0.90413 0.98462 0.98452 0.9787 0.9787 0.9787 0.9787 0.9787 0.9787 0.9787 0.9787 0.9787 0.9951 0.94145 0.94574 0.94575 0.95595 0.95757 0.95595 0.95757 0.95595 0.957570 0.957570 0.957570 0.95757000000000000000000000000000000000	0.00729 0.07207 0.07237 0.07237 0.07237 0.07237 0.0093 0.0789 0.0717 0.00808 0.00808 0.00707 0.00729 0.00729 0.00737 0.00737 0.00737 0.00737 0.00737 0.00737 0.00737 0.00738 0.01184 0.01184 0.01196	0.0022 0.00317 0.00317 0.0030 0.0028 0.0043 0.0028 0.0043 0.0027 0.0020 0.00270 0.00270 0.00270 0.00	0.05200 0.22523 0.05231 0.05231 0.0525 0.0811 0.0525 0.0811 0.0525 0.0810 0.0709 0.05 0.0709 0.05 0.0709 0.05 0.0709 0.05 0.0501 0.0501 0.0501 0.0525 0.0410 0.05433 0.04151 0.05433 0.04151 0.05476 0	0.00313 0.02703 0.00317 0.00303 0.0031 0.0031 0.0043 0.0043 0.0043 0.0044 0.0045 0.0045 0.0045 0.0054 0.0054 0.0054 0.00313 0.00254 0.00313 0.00254 0.00313 0.00254 0.00315 0.002550 0.002550000000000	32 36 36 34 31 34 31 22 29 predi at 31 31 33 34 41 32 39 36 6 31 33 33 33 33 32 23 22 32 32 32 32 32 32	19 22 17 20 25 25 17 7 7 22 CCTIO 21 21 21 20 21 21 20 21 21 20 22 23 24 18 23 22 23 24 18 23 22 24 18 23 22 24 23 22 24 24 25 25 25 25 26 25 26 26 26 26 27 27 26 26 26 26 26 26 26 26 26 26 26 26 26	7 76 82 85 77 80 70 64 92 80 70 64 92 80 70 70 70 80 70 80 70 77 77 84 84 90 83 76 84 90 83 77 84 88 83 76 84 90 83 84 80 83 84 84 85 85 80 70 70 70 70 70 70 70 70 70 70 70 70 70	400 369 374 411 372 425 390 419 odel ar longa 430 414 395 414 395 401 427 388 401 427 382 382 382 382 385 385 385 385 385	633 602 578 645 578 650 650 650 654 654 654 654 654 654 654 654 655 655	21 19 28 19 21 21 21 21 21 17 26 7 20 20 20 20 20 20 20 20 20 20 20 20 20	20.6539465 22.17530654 23.1512442 22.172482 22.172482 22.172485 22.172485 22.172485 22.172485 22.0716422 20.178552 20.178552 20.178572 20.178572 20.178572 20.178772 21.4853267 21.4853267 21.4853267 21.4853267 21.0954725 21.095475 21.095	0.3590 9.7590 9.7590 0.84871 4.8400 1.74274 2.76675 2.76675 2.76675 2.76675 2.76675 2.76675 4.73552 9.8915 4.73552 9.8915 4.73552 9.8915 4.73552 9.73554 4.65712 4.55712 4.557
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$\begin{array}{c} 97\\ 98\\ 99\\ 100\\ 101\\ 102\\ 103\\ 104\\ 105\\ Fign\\ 106\\ 107\\ 108\\ 107\\ 108\\ 107\\ 108\\ 107\\ 108\\ 107\\ 109\\ 100\\ 110\\ 111\\ 112\\ 113\\ 114\\ 113\\ 114\\ 113\\ 114\\ 112\\ 112\\ 112\\ 123\\ 124\\ 125\\ 126\\ 126\\ 127\\ 128\\ 128\\ 128\\ 128\\ 128\\ 128\\ 133\\ 134\\ 135\\ 135\\ 135\\ 135\\ 135\\ 135\\ 135\\ 135$	0.9879 0.9809 0.98442 0.98462 0.98462 0.98462 0.9875 0.7095 0.9787 0.7095 0.94762 0.94764 0.98678 0.98737 0.7086 0.98682 0.98737 0.7086 0.98682 0.98737 0.708682 0.98682 0.98682 0.98688 0.98736 0.98688 0.98736 0.98688 0.98736 0.98688 0	0.00720 0.07207 0.0121 0.0093 0.0121 0.0093 0.0121 0.0093 0.0121 0.0093 0.0171 0.0008 0.00082 0.00082 0.00082 0.00082 0.00082 0.00082 0.00082 0.00182 0.00182 0.011820	0.0028 0.0020 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0027 0.0028 0.0027 0.0028	0.08200 0.22823 0.08221 0.08241 0.08545 0.0821 0.08545 0.0821 0.08545 0.08541 0.08545 0.04038 0.04048	0.00313 0.00313 0.0031 0.0032 0.0031 0.0032 0.0031 0.0032 0.0031 0.0032 0.0031 0.0032 0.0031 0.0032 0.0032 0.0032 0.0031 0.0032 0.0030 0.0032	32 36 36 36 34 31 31 31 32 29 90 90 90 90 91 33 30 30 30 30 30 30 30 31 31 32 30 30 30 30 30 30 30 30 30 30 30 30 30	19 22 17 20 22 25 17 22 25 17 22 25 17 22 20 21 20 21 21 20 21 21 20 21 21 21 20 21 21 21 21 21 21 21 21 21 21	76 76 82 85 77 87 80 70 77 87 80 70 70 84 90 83 70 84 90 83 70 84 90 83 78 84 90 83 78 84 90 83 78 84 90 81 75 80 80 87 90 81 75 76 90 75 76 76 91 75 76 76 77 73 73 74 74 73 77 74 73 84 73 84 73 84	400 349 400 274 411 372 425 390 del ar 419 414 391 414 391 398 414 391 398 414 414 391 398 414 414 395 414 419 398 414 419 398 416 417 419 419 419 419 419 419 419 419 419 419	623 578 645 650 650 650 650 652 654 654 654 654 654 654 655 654 655 654 654	21 19 28 19 21 21 21 27 19 20 20 20 20 20 20 20 20 20 20 20 20 20	20.650445 20.52065 21.52065 21.520644 22.1272065 22.127444 22.127458 22.127458 22.0764497 22.076447 22.076447 22.076447 22.076447 20.076447 20.0764747 20.076479 20.07779 20.077779 20.0777779 20.077779 20.0777779 20.077779 20.0777779 20.0777779 20.0777779 20.0777779 20.0777779 20.0777779 20.077777777777777777777777777777777777	0.3590 0.4477 9.7530 0.4477 4.8400 0.2544 4.27677 0.2544 4.27677 0.2544 4.27677 4.29677 4.236777 4.236777 4.23677 4.23677 4.23677 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.2367777 4.2367777 4.23677777 4.236777777777777777777777777777777777777
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97 98 99 100 101 102 103 104 105 Fig 105 106 107 108 109 110 111 111 113 113 114 115 116 117 122 123 124 126 Fig 127 128 129 121 121 121 121 121 122 123 124 125 129 141 141	0.9879 0.9809 0.98442 0.98442 0.98452 0.98452 0.98452 0.9875 0.7095 0.9875 0.9875 0.9875 0.98652 0.9875 0.9825 0.9825 0.98575 0.98652 0.9825 0.98575 0.98575 0.98652 0.98652 0.98655 0.985	0.00720 0.07207 0.01221 0.0093 0.01231 0.0093 0.0123 0.0093 0.0127 0.0008 0.0016 0.0016 0.00080 0.00180 0.00180 0.00180 0.01120 0.00180 0.01120 0.00180 0.01120 0.01100 0.011200000000	0.0028 0.0020 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0028 0.0027 0.0028	0.05200 0.22523 0.02231 0.0525 0.05251 0.0525 0.0555 0.055	0.00310 0.00310 0.0031 0.0032 0.0031 0.0032 0.0031 0.0032 0.0031 0.0032 0.0031 0.0032 0.0031 0.0032 0.0031 0.0032 0.0032 0.0032 0.0031 0.0032 0.0030 0.0032 0.0030 0.0030 0.0030 0.0030 0.0030 0.0030 0.00300	32 36 36 36 34 31 31 31 32 29 90 90 90 90 91 33 30 30 30 30 30 30 30 31 31 32 30 30 30 30 30 30 30 30 30 30 30 30 30	19 22 17 20 25 17 22 17 22 17 22 17 22 17 22 17 22 21 20 21 20 21 20 21 22 23 24 18 22 23 24 18 20 20 21 22 23 24 18 21 22 24 19 20 21 22 24 21 22 24 21 22	76 76 82 85 77 87 80 77 80 70 70 84 92 89 77 77 77 77 77 84 90 84 90 84 90 81 76 84 70 84 80 767 76 84 70 84 70 84 76 87 76 77 77 78 76 76 76 76 77 73 76 74 76 77 77 73 80 77 73 76	400 349 400 274 411 372 425 380 del ar 1000ga 419 414 385 410 386 410 386 410 386 410 386 438 439 447 386 438 447 386 438 447 386 438 447 386 447 447 386 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 386 447 447 447 386 447 447 447 447 447 386 447 447 386 447 447 386 447 447 447 447 447 447 447 447 447 44	623 578 645 673 650 650 650 654 654 654 654 654 654 654 677 644 699 654 655 658 776 658 658 776 658 658 776 658 658 776 658 658 776 658 658 776 658 658 776 658 658 778 658 658 778 658 658 778 658 658 778 658 658 778 658 658 778 658 658 778 658 658 778 658 658 778 658 658 658 659 659 650 654 654 655 778 654 655 778 655 778 778 655 778 778 655 778 778 778 778 778 778 778 778 778 7	21 19 28 19 21 21 21 27 19 20 20 20 20 20 20 20 20 20 20 20 20 20	20.650445 20.52065 21.52065 21.520644 22.1272065 22.127444 22.127458 22.127458 22.0764497 22.076447 22.076447 22.076447 22.076447 20.076447 20.0764747 20.076479 20.07779 20.077779 20.0777779 20.077779 20.0777779 20.077779 20.0777779 20.0777779 20.0777779 20.0777779 20.0777779 20.0777779 20.077777777777777777777777777777777777	0.3590 0.4477 9.7530 0.4477 4.8400 0.2544 4.27677 0.2544 4.27677 0.2544 4.27677 4.29677 4.236777 4.236777 4.23677 4.23677 4.23677 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.236777 4.2367777 4.2367777 4.23677777 4.236777777777777777777777777777777777777

Figure (18-g) Testing the prediction model and calculating the mean error in predicting the elongation ratio.

148	0.98267			0.0/14/	0.00536	31	21	88	392	000	20	22.3/130121	-2.3//30
149	0.98614	0.01	0.00386	0.05717	0.00429	29	21	81	403	617	19	20.90177707	-1.901777
150	0.98845	0.00834	0.00322	0.05955	0.00357	36	20	114	386	595	25	25.6022019	-0.602203
151	0.97787	0.01716	0.00463	0.06862	0.00515	31	21	82	393	529	20	24.69501719	-4.69501
152	0.98746	0.00987	0.00267	0.0395	0.00296	32	27	72	390	607	27	21.73238452	5.267615
153 154	0.9901	0.00715	0.00276	0.05104	0.00306	34	24	74	405	624 614	24 20	20.90145116 20.49787691	3.098549
155	0.70479	0.00796	0.00307	0.01819	0.00341	33	23	82	431	670	18	18.84456498	-0.84456
156	0.75556	0.00745	0.00287	0.01703	0.00319	34	16	82	437	686	20	19.28204853	0.717951
157	0.5735	0.01096	0.00228	0.05482	0.00253	30	22	76	374	602	21	21.0724362	-0.07243
158	0.98501	0.01204	0.00296	0.06129	0.00328	31	19	77	381	603	20	23.5630849	-3.56308
159	0.95664	0.00936	0.00281	0.04159	0.00312	29	22	81	432	642	18	21.49161104	-3.49161
160	0.76112	0.00761	0.00294		0.00326	34	23	86	461	743	17	20.41166322	-3.41166
161	0.30963	0.00834	0.00322	0.05359	0.00325	32	19	23	362	581	20	12.51230239 25.01738091	7.48769
163	0.66688	0.00753	0.0029	0.05378	0.00323	29	18	87	394	627	23	19.54074274	3.45925
164	0.60024	0.00934	0.0036	0.04402	0.004	24	17	76	400	615	19	16.83728798	2.16271
165	0.8588	0.0071	0.0027	0.0404	0.003	30	22	75	430	686	18	19.20545145	-1.20545
166	0.9691	0.0073	0.0028	0.0417	0.0031	37	23	75	438	667	19	21.11069925	-2.11069
167	0.9677	0.0076	0.0029	0.0435	0.0033	32	25	79	468	755	16	20.69968733	-4.69968
168	0.9368	0	0.0632	0.2342	0.0703	32	15	80	479	717	15	-71.35757204	86.3575
Fig	ure (18-h							odel aı elonga			ting the	mean
169 170	0.98787	0.00875	0.00338	0.06252	0.00375	29 34	20	77	456 417	778	17 19	20.67305486 20.13003091	-3.67305
171	0.9891	0.00787	0.00303		0.00337	27	19	72	410	663	19	19.10609435	-0.10609
172	0.98934	0.00769	0.00297	0.04397	0.0033	26	22	75	455	707	17	19.38705749	-2.38705
173	0.73551	0.00686	0.00265	0.03923	0.00294	28	23	72	513	778	16	17.78666552	-1.78666
174	0.97761	0.00796	0.00307	0.04547	0.00341	33	24	77	462	666	16	20.78558578	-4.78558
175	0.9901	0.00715		0.05104	0.00306	30	21	73	459	698	17	20.10245742	-3.10245
176	0.98979	0.00722		0.05155	0.00309	32	23	73	433	656	20	20.46457904	-0.46457
177	0.986	0.01	0.004	0.05716	0.00429	28	17	68	420	691 697	20	19.21993525 19.91116592	0.78006
179	0.97914	0.0149	0.00596	0.08514	0.00639	28	19	92	364	553	22	22.40176382	-0.40176
180	0.98383	0.01167	0.0045	0.0667	0.005	34	20	82	419	634	19	22.14584951	-3.1458
181	0.98934	0.00769	0.00297	0.05496	0.0033	32	20	73	397	681	22	20.56388397	1.43611
182	0.99069	0.00788	0.00143	0.05629	0.00338	23	18	64	479	762	17	20.04526497	-3.04526
183	0.6462	0.01346	0.00377	0.05385	0.00404	34	15	103	374	639	22	24.15270361	-2.15270
184	0.97349	0.02071	0.0058	0.06214	0.00621	32	23	97	425 426	661	19 19	26.55501935	-7.55501
185	0.99698	0.0071	0.00285	0.0407	0.00305	29 24	17	80	426	660 673	19	22.30298019	-3.3029
186	0.9901	0.0071	0.0028	0.0408	0.0031	24	1/	80	414	706		19.46110202	1.53889
188	0.4354	0.0096	0.0029	0.0637	0.0032	29		76		747	18	19.2252696	-1.2252
188							21 27	83	443		18	20.54781477	-2.54781
	0.667 ure (0.0111 18-i) Tes	sting			iction	n mo				20.11220753 ting the	-3.11220 mean
190	0.00000	0.00070	0.00293					the e	longa	tion 672		23.81384107	-4.81384
190		0.00976				39 30	21 17	73	423 402	605	19 19	19.19603686	-0.19603
191	0.98979			0.04207		33	20	77	402	726	19	20.75527761	-0.19603
	0.98968			0.04212			1000	81			17		
193						30	24		444	606		20.65891213	-3.65891
194		0.00926		0.04116		30	22	72	437	703	18	20.90057317	-2.90057
195	0.7475	0.00769			0.0033	30	17	82	448	744	17	19.37208998	-2.37209
196	0		0.01001			31	27	88	378	610	21	20.03699016	0.96301
197	0	0.03186	0.01229	0.22758	0.01365	30	16	76	433	787	18	19.90216066	-1.90216

148 0.98267 0.01251 0.00482 0.07147 0.00536 31 21 88 392 635 20

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22.37730121 -2.377301

Average Prediction Error = - 1.153241

Figure (18-i) Testing the prediction model and calculating the mean error in predicting the elongation ratio.

From Figure (18) the prediction process for the elongation ratio was carried out for 197 samples and the average error was very small 1.153241 - compared to the sample size 197 and the mean error sign was negative and this indicates that the real value is smaller than the prediction value, so we increased the average error to the prediction to get the mean error equal to zero.

3.5. Prediction Facilitation Model for Mechanical Properties:

To facilitate the prediction process, we made a model shown in Figure (19) to calculate the mechanical properties of iron for 10 samples at once from cells introducing chemical additives and cells for predicting mechanical specifications, and this is because the LISCo does 10 diets per day.

	_ 1	nput		For Ch ditives	emic	al			ed Mechar ecifications	
DRI	FeMn	FeSi	Lime	Dol.	С	Si	Mn	جهد الخضوع	قوة الثد	الاستطالة%
0.7958	0.0101	0.0027	0.0403	0.003022	29	21	76	407.9867174	634.4847658	20.54781477
0.667	0.0111	0.0043	0.0635	0.004764	33	27	83	435.8850129	730.4449011	20.11220753
0.9331	0.0098	0.0029	0.0434	0.003255	39	21	87	396.7607883	724.9590273	23.81384107
0.7784	0.0084	0.0028	0.0421	0.003156	30	17	73	401.6996346	591.018618	19.19603686
0.9898	0.0074	0.0028	0.0421	0.003159	33	20	77	405.1409158	663.5611413	20.75527761
0.9897	0.0074	0.0029	0.0426	0.003193	30	24	81	421.3688381	704.9184526	20.65891213
0.988	0.0093	0.0028	0.0412	0.003087	30	22	72	406.2842606	649.1640521	20.90057317
0.7475	0.0077	0.003	0.044	0.003298	30	17	82	407.2701825	622.2687546	19.37208998
0	0.026	0.01	0.1854	0.011123	31	27	88	437.0503779	677.7939577	20.03699016
0	0.0319	0.0123	0.2276	0.013655	30	16	76	390.9556703	514.6043996	19.90216066

Figure (19) Model to facilitate prediction of mechanical properties. **3.6. Matching Model:**

To facilitate the prediction process, we made the model shown in Figure (20) for the cells for the quality of the products and their conformity with the specifications approved by the LISCo, where the model puts a mark (OK) if the prediction is within the acceptable limits, and a mark (Rejected) if the prediction is within the limits rejected.

	Qua	inty Mechanical Products	Quality of
Subjection	Stress	Tensile Strength Quality	Elongation Ratio
OK		ОК	OK
OK		OK	OK
OK		OK	<u>OK</u>
OK		OK	OK
OK		OK	<u>OK</u> OK
OK		OK	OK

Conclusion:

From the results and prediction models of this study, we can conclude the following:

- 1. The LISCo's lack of knowledge of the importance of prediction models for mechanical properties that reduce uncertainty.
- Through the use of the model in forecasting, prediction values 2 were obtained that are very close to the real results of the mechanical properties of longitudinal rolling iron for iron and steel plant.
- Obtaining an error rate close to zero in the process of predicting 3. the mechanical properties of longitudinal rolling iron for the iron and steel plant, and this increases its accuracy.
- 4 Such model lead to save time and contribute in cost reduction as compared to the traditional tests that used to ensure the quality of mechanical properties.
- The possibility of modifying the chemical composition of the 5. mixture to obtain the required mechanical specifications before the manufacturing process and the production of out-of-spec products.

Recommendations:

Through this research, we can recommend the following points:

- Emphasis on the importance of applying the forecasting process 1. in decision-making as a method for building the future and reducing costs for the organization.
- Emphasis on the importance of statistical modeling using 2. forecasting modeling techniques in calculating expectations.
- We recommend paying attention to databases and previous 3. statistical information in order to serve the planning process satisfactorily.
- 4. The higher the efficiency of the predictive operations of the LISCo, the closer the picture will be to the desired reality requested by the institution.
- 5. Developing statistical and planning training methods and methodology for preparing plans and formulating decisions in order for the LISCo to keep pace with recent developments in the administrative, economic and social sciences.
- The use of programs for the forecasting process, such as the 6. mechanical specifications of the company's products in various other products, which allows the company to increase its production by reducing the percentage of rejected products that are out of specifications.
- The use of this model, which was prepared to predict the 7. mechanical specifications of the company's longitudinal rolling products, and whose predictive ability has been proven through that the average error is almost equal to zero, before the manufacturing process, which leads to an increase in the company's productivity, reduces the percentage of rejected and raises the quality of its products.

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